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ENGINEERING ELEMENTS OF EXPLOSIONS

Ny.

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RACT. Two rather distinct types of blast are generated in the crainery throughere in a conventional explosion. One is a alone in composite blast that involves both evolusion products and air; the other is a more remote blast that two atmospheric air only. These two tyres of blast are described qual. Evely and quantitatively in terms of a reference explosion, chosen here as that of a bare spherical charge of unit mass of Till in the ordinary atmosphere. The scaling lava for explosions which are geometrically similar are deduced from basic principles, and their limitations campfully outlined. Representative applications are illustrated by numerial examples. The transient nature of blast is one of its important aspects and makes it difficult to establish its large potential by analytic means in ac. except the simplest circumstances. Hence, there is still need for semi-empirical mathods auch as one based on critical impulse delivered within a critical time. Detailed tables for characteristics of blast from reference explosions (Appendixes A and B) give values for peak overpressure, impulse, decay characteristics, and travel and duration times, all as a function of distance and for both free-field and normal reflection situations.



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INTRODUCTION

Explosion damage is a consequence of energy transfer from explosive to target. Mechanisms for this energy transfer are afforded both by missiles and by blast, the relative importance of which depends on circumstances. Missiles such as a rifle bullet or shrapnel are effective devices for transfer of energy, particularly when a limited amount of this energy is available. For large explosions or for area targets, blast may well be a major mechanism for explosion damage, and is also of concern in distributed energy explosions and with weapons that achieve a focused blast effect. In addition, blast is important in connection with the safety aspects of explosives, with disaster recovery planning, and in any situation where protection against explosions is required.

To outline briefly the nature of blast, the sudden expansion of originally highly compressed explosion products generates the blast wave. For a conventional explosive in the ordinary atmosphere, the close-in blast involves both these expanding products and the air that they are pushing back. This air is compressed in the push-back process, and so acts to retard the expanding products and to extend the disturbance. The air portion of the blast outruns the products portions, and at some distance from the explosion the blast involves atmospheric air only. There are then two types of blast waves, those close-in that are of composite nature and involve both explosion products and atmospheric air, and those further out that involve atmospheric air only.

The two types of blast waves are conveniently described in terms of a reference explosion, chosen here as that of a bare spherical charge of TNT in the ordinary atmosphere, a situation for which there are detailed analytic calculations (Ref. 1 and 2) and confirming experiment measurements (Ref. 3-5).

DISCUSSION

SHOCK FRONT OF A BLAST WAVE

The sheath of highly compressed air surrounding the central core of expanding explosion products moves out from the explosion it supersonic speed. A pressure jump, or pressure discontinuity, marks its leading surface. This discontinuity is the shock front for the explosion. For

the reference explosion, the initial jump in pressure of the surrounding atmosphere occurs at the charge surface and has a value of about 450 bars (about 5,500 psi). The intensity of this pressure jump decreases rapidly with distance out from the center of the explosion, and approaches zero for infinite distance. This pressure jump is referred to as the "peak everywasure" for the explosive blast ways.

There appears to be no simple analytic expression that adequately describes behavior of the peak overpressur; with distance from the center of the explosion. However, it may be noted that the peak overpressure decreases with a maximum of eight-thirds power of the distance at moderate distances such as 20 charge radif from the explosion, and that both closer in and further out the exponent expressing the rate of decrease is smaller. At remote distances from the explosion the peak overpressure is inversely proportional so the first power of the distance. This is the behavior of a sound wave. Herea, it may be said that any explosive blast eventually degenerates into a sound wave, which is the characteristic sound of an explosion far away.

PRODUCTS-AIR INTERFACE

The tremendous unbalance between explosion pressures and those of the surrounding atmosphere serves to accelerate drastically the perimeter portions of the products of detonation. The resulting motion of this material is a primary mechanism for generation of the atmospheric disturbance. As these rapidly moving products impinge on surrounding air, their motion is impeded and their forward momentum transferred to the air. The location at which forward motion of products ceases is a basis for distinguishing between composite blust and simple air blast. For the reference explosion the distance for maximum excursion of products is about 16 charge radii, or about 95 centimeters for the explosion of 1 kilogram of TMT (2.4 feet for 1 pound). The peak air shock overpressure experienced previously at this distance is about 12 bars (about 175 psi) in the standard atmosphere. Also, the mass of air displaced by explosion products becomes somewhat more than three times the mass of the explosive.

At the interface between products and air, the pressure accreases from an initial value of about 450 bars at the charge surface down to atmospheric pressure at its maximum excursion distance. However, this interface cannot be located as definitely as this discussion implies. The expanding explosion products form a roiling cloud, and contact between products and resisting atmospheric air occurs in a turbulent interaction-transition zone rather than at an infinitely thin contact surface (Ref. 6). An important aspect of this turbulence is that it becomes difficult to assign precise characteristics to the expanding explosion products.

Hence, classical characteristics of an explosion, as quoted here or alsowhere, should be regarded as representative rather than as definitive. Furthermore, the turbulent nature of the contact zone makes the interface

appear to extend further than the distances computed on the basis of sharp discontinuity. Also, explosion products from an oxygen deficient explosive such as TNT may react with oxygen from the air to produce an apparent extension of the contact zone.

PRODUCTS CLOUD

Pressure initially within the explosior products is detonation pressure. For TNT, detonation pressure is a maximum of about 177 kilobars at theoretical loading density of 1.65 g/cc, about 160 kilobars at an achievable 1.615 g/cc, or about 148 kilobars at nominal loading density of 1.50 g/cc. The central por ion of this products cloud expands more or less directly in place, and here the pressure decreases in accordance with the isentropic pressure-volume relation. As this cloud expands it engulfs the immediately surrounding volume, producing pressures which may very well exceed those at that location produced by the previously passing air shock front. Direct explosion pressures exceed shock-generated pressures out to about 1.6 charge radii, where the peak is about 550 bars (about 5,000 psi) in the ordinary atmosphere. This particular distance thus distinguishes between the region of direct explosion effects and the region of blast-wave effects.

To summarize these pressure regions, direct explosion pressures in the ordinary atmosphere involve distances less than about 1.6 charge radii from explosion center and peak overpressures greater than about 350 bars (5,000 psi). The region of composite blast extends out to about 16 charge radii or more, with peak overpressures between 350 and 12 bars (5,000 psi and 175 psi). Simple air blast occurs at distances greater than this nominal 16 charge radii and shows peak overpressures less than 12 bars (175 psi) for the reference explosion in the ordinary atmosphere.

STRUCTURE OF COMPOSITE BLAST WAVES

The relatively complicated pressure structure for a composite blast wave is shown in Fig. 1. Outermost is the shock with its accompanying peak overpressure, and within it there is an air sheath surrounding the explosion products. Next is a layer of recompressed explosion products that have been decelerated by impact with the air sheath. Within this is a zone of repidly moving products at a lower pressure, and then a centrally located products cloud. For the particular time shown in Fig. 1, the air shock (S_1) is at a distance of 5 charge radii from explosion center. The contact surface or products-air interface, (C.S.), is at about the charge radii, and the shock-wise deceleration (S_2) of products impinging on previously decelerated layers, the so-called second shock, is just within this distance.

Figure 2 shows profiles for additional items at this particular time. Discontinuities at both the air shock and the second shock are shown in

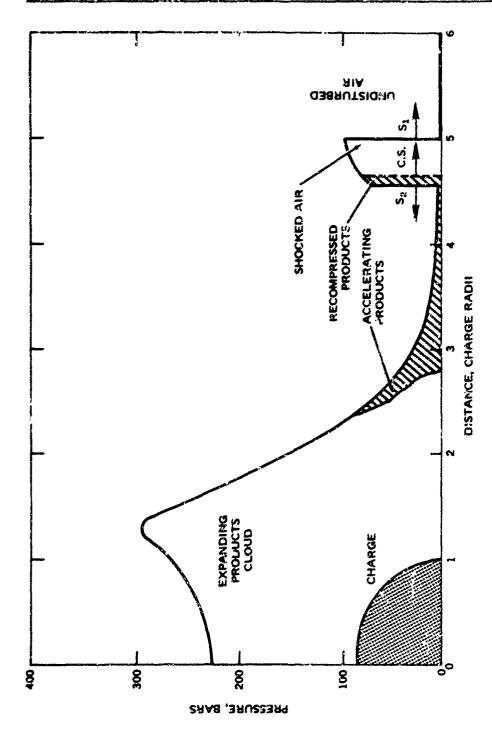


FIG. 1. Pressure Profile When Shock Front is at 5 Charge Fidit.

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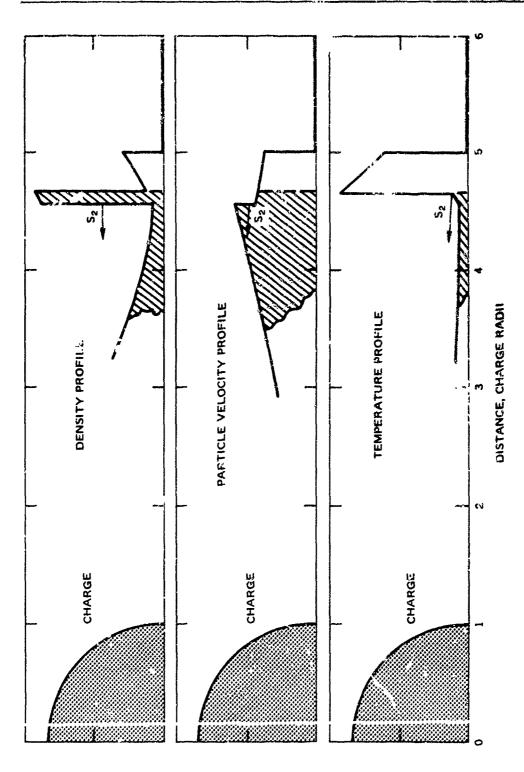


FIG. 2. Density, Particle Velocity, and Temperature Profiles.

all these profiles. However, the profiles for the pressure and particle velocity exhibit continuity at the products-air interface and only the temperature and density profiles show discontinuity. (The computations which provide the data for these profiles have made suitable allowance for both nonideal gas behavior and for variation of specific heat with temperature.)

BLAST-WAVE DURATION

The pressure profile for a composite blast reaching out to 11 charge radii from explosion center is shown in Fig. 3. At this time pressures in the central products cloud have become less than those generated at the shock front. Worded alternatively, rarefaction has progressed back through the explosion products. Also at this time a negative pressure phase, one with pressures less than atmospheric, appears inward of the second shock in the accelerating products.

Appearance of a negative pressure at any location limits the time duration for the positive pressure phase. For the reference explosion this negative pressure appears first at a distance of about 9 charge radii from explosion center and so this distance also marks the location of a minimum time duration for the positive phase. Closer in, pressures in the products cloud persist for longer than minimum time, and further out the air sheath is thicker and travels slower, hence its positive pressure at a given location persists for a longer time.

Precise values for a duration of the positive pressure phase of any explosive blast (and its negative phase as well) are rather difficult to establish experimentally. Close in, the turbulent nature of the products cloud reduces the significance of any individual value, and further out a slow pressure subsidence of the less intense blast waves allows inherent random fluctuations to obscure the measurements.

AIR BLAST FROM AN EXPLOSION

The pressure profile for a blast-wave system that extends out to 25 charge radii from explosion center is shown in Fig. 4. At this particular time the explosion products have reached their maximum calculated excursion of 16 charge radii, and the pressure at the products-air interface is now atmospheric. Pressures within the products region, including those generated in the second shock, are now all less than atmospheric. Pressures in the air sheath extending from air-products interface out to the shock front are all above atmospheric, and form a region of positive overpressure with relatively simple structure.

The pressure profile for the blast wave when the shock front disturbance has reached still further out to 50 charge radii is shown in Fig. 5.

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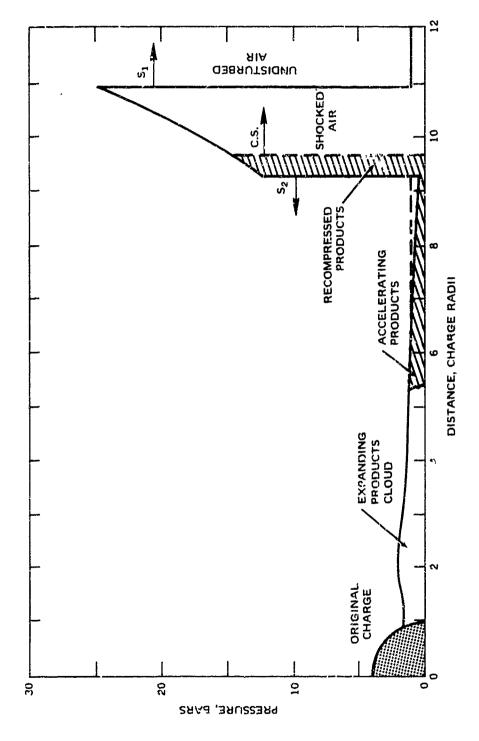


FIG. 3. Pressure Profile When Shock Front is at 11 Charge Radii.

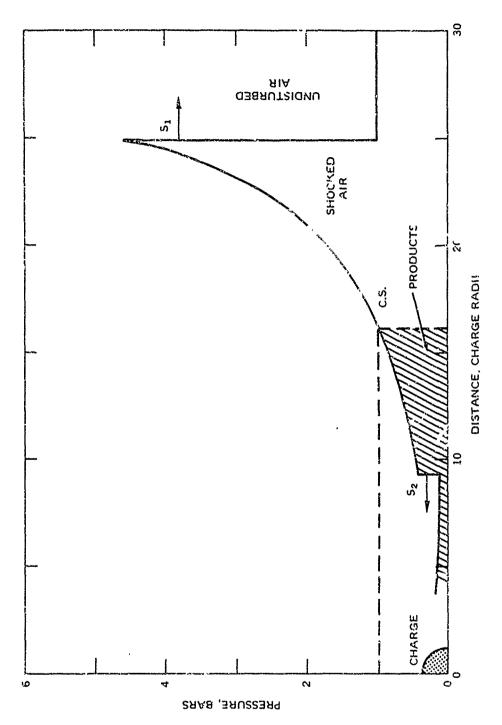
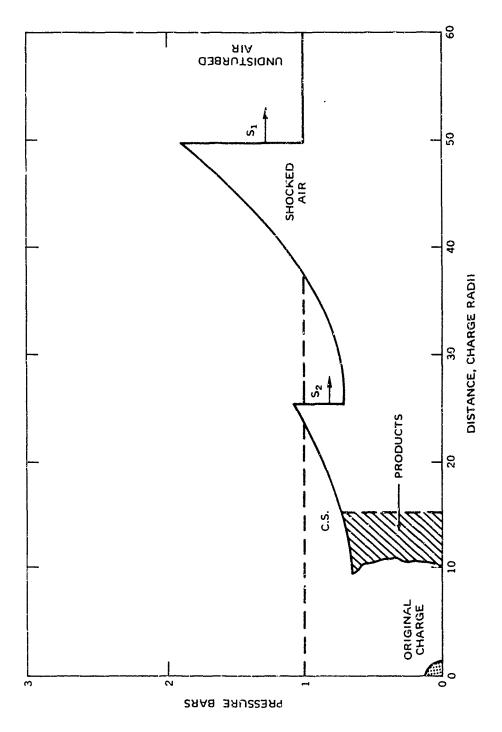


FIG. 4. Pressure Profile for Shock Front at 25 Charge Radii.



IG. 5. Pressure Profile for Shock Front at 50 Charge Radil.

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Here, also, the initial positive pressure phase involves only air from the atmosphere and the air blast is relatively simple in structure. Closer in, where both products and air are involved, the situation is more complex. The second shock by now has retreated to explosion center and been reflected back by the consequent implosion. Passing through the products-air interface, the density discontinuity and associated impedance mismatch at that interface causing a rarefaction disturbance, and following shock, move inward through the products. This shock then implodes at the center, etc., and these processes repeat until all the explosion energy has been dissipated. The magnitude of these supplementary shocks is small, and is further diminished by turbulence in the products cloud. These complex effects thus have little damage potential and ordinarily are disregarded in blast-damage studies.

Figure 6 is a summary, to log-log coordinates, of the pressure-distance relations for air-shock front, the products-air interface, and for the direct pressures of the expanding products cloud, all for the reference explosion. It also indicates the pressure-distance contours for several successive times t_1 , t_2 , t_3 , and t_4 after the instant of explosion.

TIME-OVERPRESSURE RELATIONS FOR AIR BLAST

Related to the pressure-distance relations for a given time after explosion is the overpressure-time relation at a given location, for this pertains directly to blast damage potential and to experimental blast-wave measurements. A typical overpressure-time relation for a specified distance is shown in Fig. 7. This is for the free-field overpressures at various times at a distance of about 25 charge radii from the reference explosion. Its peak overpressure is 3.6 bars, and for a 1-pound charge of TNT this occurs about 0.8 milliseconds after the instant of explosion. The overpressure then decays to zero in a duration of about 0.70 milliseconds additional time (for this charge). For comparison with this theoretically calculated curve, Fig. 8 shows two actual overpressure-time records (but not to the same scales).

The relatively simple structure of these blast waves permit their description in terms of simple numbers. General appearance suggests an exponential relation, but the overpressure goes negative in finite time, a behavior not accommodated by a simple exponential. An empirical adjustment is readily made, however, to give a relation that adequately describes the positive overpressure phase of the air blast. This gives

$$p = p^{0}(1 - t/t_{d})e^{-bt/t_{d}}$$
 (1)

where p is the overpressure at time t which decays from its peak value p^{O} at zero time to zero value at duration time t_d . The item b, the decay

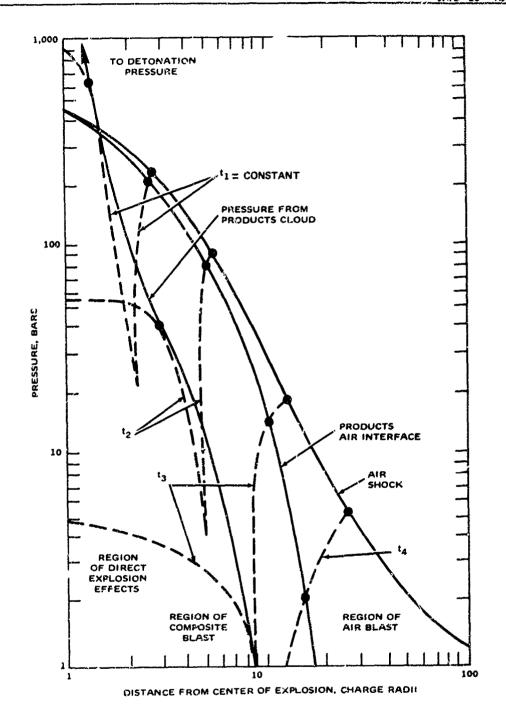
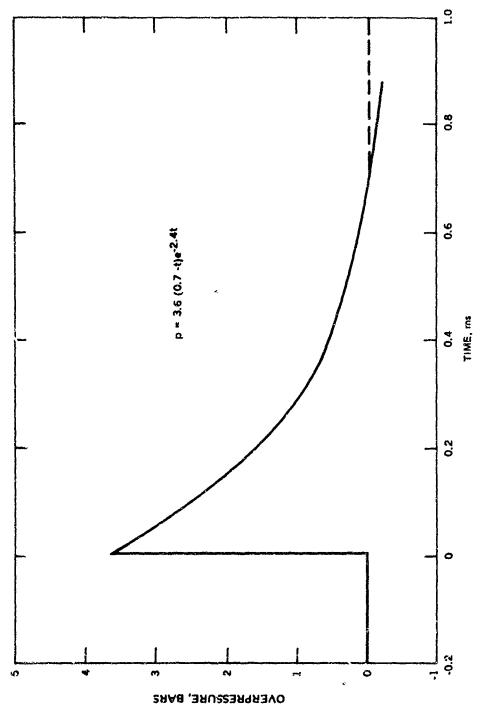
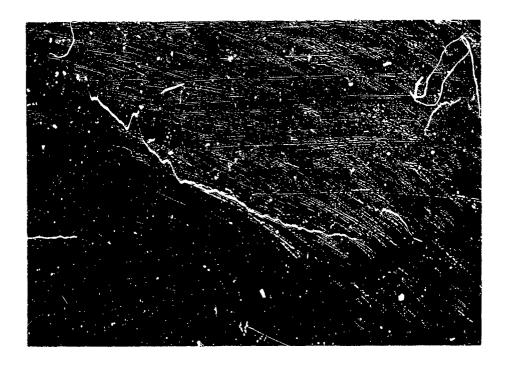


FIG. 6. Fressure-Distance-Time Relations for Reference TMT Explosion.



7. Time-Overpressure Relations for Representative Simple Air Blast.



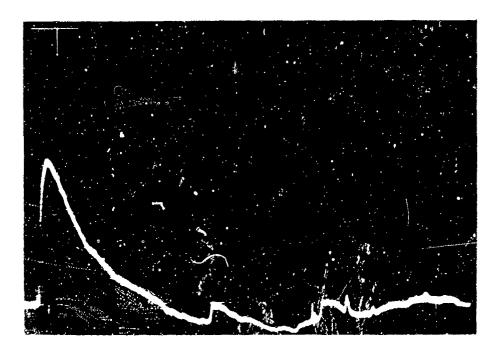


FIG. 8. Actual Overpressure-Time Records. Upper record is with high impedance gage; lower with low impedance gage.

parameter, is analogous to a rate constant. Its value varies with distance from the explosion, decreasing from a maximum of about 4.17 at the nominal 16 charge radii marking the beginning of simple air shock down to a value of about 0.9 at around 40 charge radii. It decreases to still lower values at more remote distance as the blast wave becomes distorted with distance and presumably approaches the triangular at the more remote distances. The triangular blast wave corresponds to zero decay parameter; it is of interest to note that much of the earlier theoretical work onblast assumed a triangular blast wave. Currently, for an approximation, the value unity is assigned to the decay parameter for all distances; the insensitive nature of the relation makes this a quite acceptable approximation for many purposes.

The analysis of measured time-overpressure relations and the assignment of values to the decay parameter are considered later. However, note that the dimensionless nature of the decay parameter b of Eq. 1 makes its values apply directly to all the various systems of units used in blast-wave studies.

For the close-in composite blast wave there is no simple analytic expression for its time-overpressure relation, and any expression such as the above is at best only an approximation. This composite shock not only involves two materials, products and sir, but also pressure discontinuities such as the second shock, and here a graphical presentation of shock characteristics is indicated.

PLAST IMPULSE FER UNIT AREA

The impulse characteristic of a blast wave is the total momentum charge per unit area of blast surface. It is an important parameter in the study of blast dawage potential. The positive impulse per unit area is given as the time integral of the (positive) blast overpressure. For simple air blast, where the positive overpressure-time relation can be described analytically by Eq. 1, this integration provides

impulse =
$$\int_0^{t_d} p \, dt = p^0 t_d [(1/b) - (1-e^{-b})/b^2]$$
 (2) (per unit area)

For the blast wave shown above, with peak overpressure 3.6 bars, duration 0.70 millipeconds, and decay parameter 1.7, the positive impulse per unit area is computed by Eq. 2 as 0.077 bar-milliseconds.

Impulse characteristics are ordinarily included as part of the com-plete description of a blast wave, for example the 0.077 bar-milliseconds
(Fig. 7) above. In addition to such direct specification there are available two alternative indirect methods. One is through the decay parameter,

for in Eq. 2 this defines the impulse when peak overpressure and time duration are known. The other indirect method is as a fraction of the square-wave impulse value (product of peak overpressure and duration). This indirect item is also dimensionless, and in the instance above this fraction is about $0.0?7/(3.6 \times 0.7) = 0.30$. This fraction varies from a minimum of about 0.17 for the rapidly decaying wave formed at the demarcation between composite blast and air blast where decay parameter b equals about 4.7. up to a limiting value of one-half for remote distances where the blast wave approaches the triangular as the decay parameter approaches zero. Values for these and other impulse factors have been completed and are listed below. Of these two alternative methods for describing the impulse of a blast wave, the one in terms of decay parameter has the advantage over the fraction of square waves impulse in that the decay parameter also specifies the entire time history for the positive overpressure phase. This provides additional information useful in a detailed study of target interaction and damage potential of the blast.

Decay parameter Fraction of square b impulse val	
0.0 0.500	
0.2	
0.4	
0.6	
0.8 0.390	
1.0 0.368	
1.2 0.348	
1.4 0.330	
1.6 0.313	
1.8 0.298	
2.0 0.284	
2.5 0.253	
3.0 0.228	
3.5 0.207	
4.0 0.189	
4.5 0.173	
5.0 0.160	

The impulse characteristic of composite close-in blast is much more complex than that for simple air blast. For example, at distances of about 10 charge radii from the TNT explosion the free-field impulse of the composite blast actually increases with increasing distance. Direct values for the close-in impulse per unit area obtained by time integration of the complex overpressure-time relation can be expressed simply in dimensionless form as a fraction of the square-wave impulse value. For composite blast this fraction decreases from about one-half at the charge surface down to a minimum of about 0.06 at about 3 charge radii, goes through a maximum of nearly one-half at the distance for minimum blast

duration, and then decreases down to about 0.17 at the 16 charge radii that marks the maximum excursion of explosion products.

REFERENCE EXPLOSIONS

Nominal values for the various characteristics of arbitrarily selected reference explosions are given in Appendixes A and B. Appendix A is based on the explosion of 1 kilogram of TWT in ordinary air at a temperature of 15 Celsius (59°F) and a pressure of 1 bar. Appendix B is for the explosion of 1 pound of TWT in air at 59°F and 13.6 psia (typical conditions for this Center). These values tabulated for reference explosions can be applied to realistic situations by means of the scaling laws as described below.

SCALING LAWS FOR EXPLOSIONS

Scaling laws for explosions are based on the principle of geometrical similarity and on the observation that the spatial dispersion of explosion energy is a volume effect. Thus doubling a distance from an explosion increases the volume of medium thected by a factor of eight, hence eight times the explosion energy (explosive yield) is required to achieve a similar blast. To allow also for the influence of the nature of the surrounding medium on this energy dispersal, note that the transfer of momentum from expanding explosion products to surrounding medium is a mass effect. Hence, energy release per unit mass of surrounding medium is a controlling item. In this study, atmospheric density is used as a measure of the relative mass of the atmospheres in which explosions may occur.

To apply these concepts, define a "scaled distance" as the equivalent distance from a reference explosion, one that corresponds to some actual distance from some actual explosion. From basic considerations

(3)

Representing the yield as W and atmospheric density as ρ , and with subscript c to identify the reference explosion, Eq. 3 can be rewritten as

scaled distance =
$$\frac{(\text{actual distance}) \times (\rho/\rho_0)^{1/3}}{(W/W_0)^{1/3}}$$
 (4)

or for the ordinary atmosphere at absolute temperature T and absolute pressure ${\tt P}$

scaled distance =
$$\frac{(\text{actual distance}) \times (P/P_0)^{1/3}}{(W/W_0)^{1/3} \times (T/T_0)^{1/3}}$$
(5)

By an analogous sort of reasoning, it may be shown (Ref. 7) that the scaled distance as so defined also carries within it a definition of scaled time. That is

scaled time =
$$\frac{(\text{actual time}) \times (\rho/\rho_0)^{1/3} \times (a/a_0)}{(W/W_0)^{1/3}}$$
 (6)

where a represents the speed of sound in the actual atmosphere and a_0 that in the reference atmosphere. In the atmosphere, this speed varies with the square root of the absolute temperature, so that Eq. 6 may be rearranged to give

actual time =
$$\frac{(\text{scaled time}) \times (\text{W/W}_0)^{1/3}}{(\text{P/P}_0)^{1/3} \times (\text{T/T}_0)^{1/6}}$$
(7)

The impulse characteristic of a blast wave, that is, its positive impulse per unit area, also follows the scaling laws. Defining scaled impulse as the value for a reference explosion and actual impulse as that for some other amount of explosive in some other atmosphere, the two are related as

Expressed symbolically, and combining with Eq. 7

actual impulse = scaled impulse x
$$\frac{(W/W_0)^{1/3} \times (P/P_0)^{2/3}}{(T/T_0)^{1/6}}$$
 (9)

These definitions of scaled distance, time, and impulse involve ratios of absolute values for atmospheric pressure and temperature raised to a fractional power. In many circumstances this gives numerical values that do not differ greatly from unity. When one considers the considerable uncertainty in measurements on any actual explosion, it becomes apparent that these ratios often may be taken as unity without introduction of additional error. This makes for a desirable simplification in formulas

for the scaling laws. Furthermore, measure explosive yield in relative rather than in absolute terms such as the energy release implied above. That is, our reference explosive yield can be that of unit mass of some reference explosive. As a reference explosive, TNT has desirable aspects of being reproducible, relatively safe, inexpensive, and readily available in calibration amounts. The value for the reference yield W₀ then becomes unity, and value for the actual yield W becomes its TNT equivalent.

In these circumstances,

(actual distance) = (scaled distance)
$$\times W^{1/3}$$
 (10)

(actual time) = (scaled time)
$$x w^{1/3}$$
 (11)

(actual impulse) = (scaled impulse)
$$\times W^{1/3}$$
 (12)

where W is effective yield in terms of the equivalent amount of TNT for the explosive whose explosion is being studied. Equations 10-12 should be regarded as merely convenient approximations for the primary forms of the scaling law as in Eq. 3, 6, and 8. Various aspects of these scaling laws are illustrated by numerical examples in the calculations of Appendix C.

LIMITATIONS OF SCALING

It is to be ϵ phasized that the scaling laws, both in original and in approximate forms, have been deduced on the basis of explosions with geometrical similarity. That is, these scaling laws apply to explosions related to each other as a photograph is related to its enlargement. Thus, in general, data on a free-field reference explosion cannot be expected to apply directly to a blast wave which has undergone the complicating effect of interaction with a ground surface, nor can a freefield explosion be scaled to one which gives shock reflections or Mach stem formation. Furthermore, there is also the requirement that two explosions to be compared must occur in atmospheres of the same general nature. Thus the scaling laws cannot be used to apply data for a reference explosion, in the ordinary atmosphere to an underwater one, not to an excatmospheric explosion of outer space. But on the other hand, most conventional explosives have about the same charge density, the same energy release, and generate about the same volume of gas per unit mass of explosive. Thus, ordinary explosions may actually meet the scaling law requirements of geometric similarity in many circumstances.

For nuclear explosions, both charge radius and products excursion distance are very small and quite different from those for a TNT reference explosion with the same energy release. Hence, these close-in effects do not scale to TNT. But for remote distances, the blast wave from either a nuclear or conventional explosive involves air only and each has the same

general behavior. An empirical adjustment can bring these two air blast waves into general conformity. Such an adjustment indicates that the effective energy release in a nuclear explosion is about 85% the actual energy release.

Another instance of inverest is the explosion of a gaseous mixture, for example that of methane and air. Lack of geometrical similarity between the large charge size of a gaseous explosive and the small charge size of relatively dense TNT means that TNT is hardly a suitable reference for gaseous explosives at close-in distances. However, at remote distances where only air blast is of concern, TNT might well suffice as reference.

Nonspherical explosions are not readily scaled to a reference spherical charge of TNT, an observation of importance in the study of focused blast explosions and in the study of blast from many types of distributed energy explosions.

For explosions in the atmosphere at high altitudes the maximum excursion of explosion products is relatively much greater than for explosions at sea level. Here the basic requirement for geometrical similarity may not be met, even for two charges of the same explosive. Hence at the very high altitudes the scaling law must be used with reservation, particularly then within the region of composite blast.

For an explosion in contact with a plane unyielding surface, the explosion energy is released into a bemisphere rather than into a sphere. Hence these blast waves may be equivalent to free-field waves generated with twice the energy release. Sind ar considerations apply to those special shock tubes where the explosion energy is concentrated into a small portion of a sphere. This gives a corresponding magnification of effective explosion yield, provided of course that the requirements of the scaling laws are otherwise met.

SCALENC LAW YIETES

An interesting application of the scaling laws for explosions is inverse of the one implied above. Here an equivalent yield from some actual explosion is computed from the characteristics of the blast wave it produces. This technique is illustrated in Appendix C. In general, the calculation first establishes a scaled distance from some characteristic of the blast wave such as its overpressure, speed of its shock front, or its positive impulse per unit area. Then by Eq. 5

$$\frac{\text{calculated yield}}{\text{reference yield}} = \left(\frac{\text{actual distance}}{\text{scaled distance}}\right) \times \frac{(P/P_0)}{(T/T_0)}$$
(13)

For the special circumstance that reference and ambient pressures and temperatures do not differ greatly, and where the reference explosion corresponds to unit yield, Eq. 13 reduces to the simple relation

calculated yield =
$$\left(\frac{\text{actual distance}}{\text{scaled distance}}\right)^{3}$$
 (14)

as illustrated in the calculations.

There are some cautionary observations to be made about calculated yield values obtained from Eq. 13 or 14. One is that the calculation involves the cube of a ratio, and this magnifies any inherent uncertainty by a factor of three. Thus these calculations are inherently of low precision. Furthermore, the yield value obtained is basically one for a spherically symmetrical explosion. Thus, it is to be anticipated that calculated values for the yield of an actual explosion may vary and depend on the type of data used in the calculation. Nevertheless, the data provide useful information for evaluation studies even if the requirements for geometrical similarity with a reference explosion are not met. This is the situation in many instances of interest such as a distributed energy explosion and focused blast. These items and calculations are in need of investigation.

EXPERIMENTAL BLAST MEASURIMENTS

Experimental measurements on blast waves are extraordinarily difficult to rake (Ref. 8). They require highly sophisticated instrumentation along with utmost care in calibration and measurement. Furthermore, incenuity sid technique are required in order to avoid spurious effects such as unanticipated reflections from the earth's surface, from the formation of a Mach stem, or from some interaction between blast wave and supporting fixtures for measuring instruments. Indeed, blast measurements are so troublesome that any individual value is always suspect. This also applies even to complete sets of measurements if all are made with the same instrumentation using the same technique. Only in individually calibrated and independently made duplicate, priplicate, or replicate measurements can full reliance be placed, and even so the inherent uncertainties should be recognized. But within such limitations the experimental measurements in blast waves from spherical charges conform quité well with data on TNT explosions as given in Appendixes A and B and as scaled up (or down) in accordance with the scaling laws.

Even with adequate instrumentation and proper calibration, any particular setup almost always involves some sort of choice or compromise. One common choice is between an instrument that is stable and reliable but slow in response, and one with a fast rise time capability but which may overshoot and be sensitive to extraneous noise. Figure 8 shows (but

not to the same scale) actual pressure records from these two types of of blast gages for the same blast wave. The lower record was obtained with a low impedance but stable pressure gage. Its reading for the instantaneous initial peak overpressure seems too low. The upper record is with a high impedance gage with considerably faster response. Here the initial peak seems well recorded, but some overshoot may be present and the entire record seems to be a noisy one.

To minimize these particular gage problems, a systematic method of smoothing experimental curves suitable for the special case of a simple overpressure-time relation without a multiple peak or incidental negative pressure portions has been suggested. This involves two semilogarithmic plots. One, for the early times of the blast, is the logarithm of the overpressure versus the time. Here back extrapolation to zero time gives a reliable value for the initial peak overpressure (see Fig. 9). The second plot is of the overpressure at later times versus the logarithm of the time, as in Fig. 10. The resulting compression of the time scale makes the curve approach linearity and permits a good estimate of the duration time for the overpressure as the time when the curve intersects the overpressure axis.

In addition to providing a smoothed value for peak overpressure and duration, the two semilogarithmic plots also establishes the decay parameter of Eq. 1. For this, note that the term $(1-t/t_{\rm d})$ of Eq. 1 approaches $e^{-t/t_{\rm d}}$ as time t approaches zero. That is, at early times Eq. 1 reduces to

$$p = p^0 e^{-(1+b)t/t}d$$
 (as $t \to 0$) (15)

Taking logarithms, then

$$\ln p = \frac{-(1+b)}{t_d} + constant \quad (as t \to 0)$$
 (16)

Comparing Eq. 16 with the formula for a straight line, it can be seen that the slope of the semilogarithmic plot (? overpressure (base e value) versus time is the negative value of the item $(1+b)/t_{\tilde{\mathbf{d}}}$. Equating and solving for decay parameter b,

$$b = -(slope) \times t_{d} - 1 \tag{17}$$

That is, measuring the intercept and slope of the plot of Fig. 9 and the intercept on the plot of Fig. 10 provides values for peak overpressure, the duration, and decay parameter. With these data the entire overpressure-time curve can be reconstructed mathematically and compared with the original measurements to provide a check on the analysis.

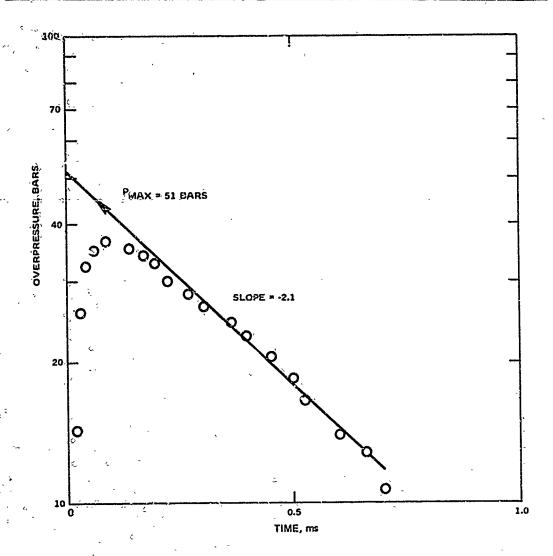


FIG. 9. Log Overpressure Versus Time. Indicated peak, 51 bars; measured peak, 38 bars. Slope is -2.1 per millisecond.

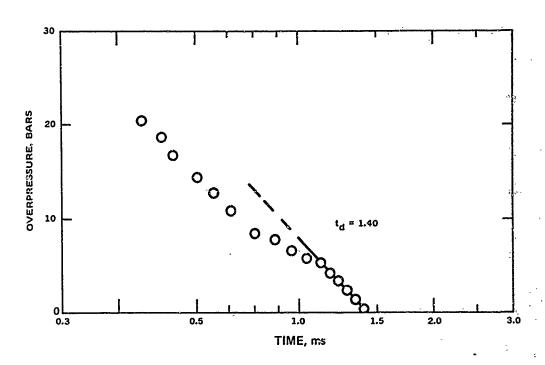


FIG. 10. Log Time Versus Overpressure. Duration 1.40 ms, decay parameter = $1.40 \times 2.1 - 1 = 1.94$.

A further check on the instrumentation and on the overall propriety of this analysis of experimental data is provided by values computed for the impulse. It has been observed that directly measured impulse values, as obtained by graphical or numerical integration of the overpressure time curve, are relatively immune to response time and noise errors. If the value for the impulse as calculated using the decay parameter agrees with the directly measured value it suggests that a reasonably reliable record of the explosion has been obtained.

DYNAMIC PRESSURE FOR A BLAST WAVE

A requirement for target damage is interaction between blast and target. One interaction effect is described by the dynamic pressure q, defined as $q=1/2~\rho u^2$, where ρ is the density of the moving stream and u its velocity. For air, the dynamic pressure may be expressed alternatively as $q=1/2~k~M^2~P$, where k is the specific heat ratio, M the Mach number for the moving stream, and P its absolute pressure. The dynamic pressure, when multiplied by a drag coefficient for some particular object, gives the drag force per unit area exerted by the moving stream on that object.

Dynamic pressures are important in steady-flow situations such as aircraft propulsion or flight of missiles. They are also of interest in

some blast situations, for example a water tank subjected to the blast wind of a nuclear explosion. But for ordinary explosions the time duration of the blast wind is relatively short and the blast-target interaction is a transient one. Here the dynamic pressure of steady flow is not particularly pertinent, and indeed it is so ill-defined physically in these explosion situations that even its direct measurement is troublesome. Rather, for dynamic blast loads in conventional explosions the important blast-target interaction is the transient one of shock reflection.

REFLECTED OVERPRESSURES

Shock reflection effects include normal reflection, oblique reflection, and Mach stem formation. The most damaging of these, at least for tough targets, ordinarily is normal reflection. For simple air blast the overpressure developed in this reflection can be established analytically. This is conveniently described in terms of a reflection coefficient, the ratio of reflected overpressure to overpressure in the free field. For distances remote from an explosion this reflection coefficient approaches two as a lower limit, as for sound waves. It increases markedly with shock intensity, reaching about 5.8 at the nominal 16 charge radii that marks the inner limit of simple air blast in the reference explosion. Corresponding peak reflected overpressure here is 5.8 x 12 = 70 bars (100 psi) versus the 12 bars for the simple side-on overpressure. It is to be recognized that overpressures such as 70 bars can be very damaging, even though of a transient nature.

Reflection effects for composite blast close to the explosion center are more troublesome to study. Reasons for this include (1) an increase in specific heat for air and for products at the high temperatures generated in these intense shocks, (2) chemical dissociation and ionization effects, (3) monideal gas behavior of the highly compressed gas in the interse shock, and (4) the finite time needed for an equilibrium distribution of energy within the shocked medium. An approximate analysis indicates that these complexities are unimportant at distances beyond about 10 charge radii, but that closer in they become quite marked. The approximate analysis also indicates the reflected impulse decreases monotonically with distance in contrast with the behavior of the side-on impulse. For the limiting situation on 1 charge radius, it is estimated that the reflection coefficient for normal reflection is about 12.2 (versus a theoretical maximum of 8.0 for the ideal gas with specific heat ratio 1.4). The calculated reflected overpressure at the charge surface becomes $12.2 \times 450 = 5,500$ bars (80,000 psi). An experimental study of these intense reflected shocks is now being planned.

BLAST LOADINGS ON STRUCTURES

In some few simple situations the load imposed by blast on a target can be calculated from fundamentals. Consider for example the blast load on the front of a disk whose surface is normal to the direction of blast-wave travel. The peak reflected transient load is the product of the peak reflected overpressure and the target area. The load decreases with time for two reasons, one the ordinary decay of the blast wave, the other a relief effect as the reflected overpressures are equalized. The decay of the blast wave has been characterized by Eq. 1. However, the reflected overpressure relief effect is an additional one superimposed on this.

With regard to the relief effect for the reflected overpressure, note that initially the reflected pressure on the face of the target is considerably greater than the pressure in the surroundings. Hence, there is flow from the face of the target into the surroundings. This relieves the reflected overpressure on the face of the target. This relief is in the form of a rarefaction wave that moves in from edge to center. Considering a particular point, the rarefaction wave arrives at some time t₁, when the pressure relief starts. This is then completed at some later time, t₂. After relief if the reflected overpressure, the disk senses only the free-field overpressure plus an incremental stagnation overpressure maintained by the impact effect of the moving blast wind.

A method of characterizing all these effects is indicated in Fig. 11 which illustrates various overpressures associated with the blast wave. The primary one of these is the side-on or free-field overpressure, but also included are the reflected and stagmation overpressures. Each varies with time, as shown. Reflected overpressure exists on the face of the disk from zero time until relief starts at time to, and the pressure after relief is completed at time to is the stagnation overpressure. The relief process cours between times to and to at intermediate pressures. Assigning representative values to $times t_1$ and t_2 based on speed of travel of a rarefaction wave and on dimensions of the disk, the blast load predicted for the center of a disk in a particular situation is that of Fig. 12. The general form of this predicted dynamic load on the front face can be compared with dynamic loads as measured at centers of a 3-inch disk and of a 9-inch disk and shown in Fig. 13. The general agreement between predicted and observed loads lends encouragement to this method of analysis, at least for simple targets.

DAMAGE POTENTIAL OF BLAST

Darage to a target from blast comes from motion of the target as imparted by forces of the blast wave. In principle, an analytic solution for target motion can be obtained from the equation of motion expressing the relation between target mass, its acceleration, and the unbalance between the driving force of the blast wave and the resistance of the

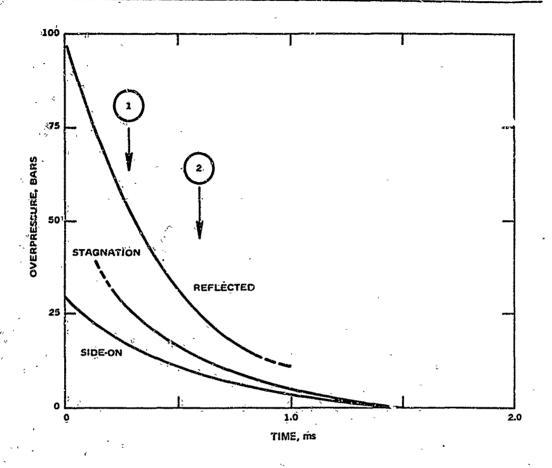


FIG. 11. Overpressure-Time Relations Needed for Determination of Dynamic Blast Load.

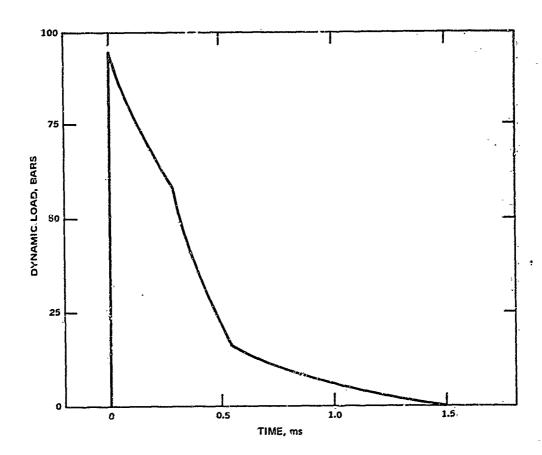
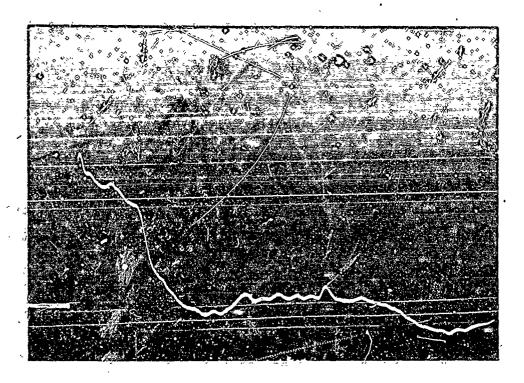


FIG. 12. Dynamic Blast Load Predicted for Center of 3-Inch-Disk 5 Feet From Reference Explosion.



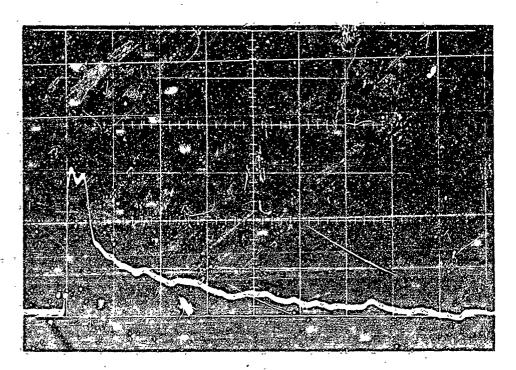


FIG. 13. Dynamic Blast Loads Measured for 9-Inch and 3-Inch Disks. (Not to same time scale.)

target. The driving force is a transient one, given as the product of target cross-section area and a blast-wave overpressure such as that of Fig. 12 or 13. The resistance of the target depends on its structural features. However, for dynamic situations this is seldom known precisely and indeed perhaps is not capable of being known. Furthermore, even if both the transient driving force of the blast wave and the dynamic resistance of the target were known, the mathematical form of the equation of motion is not conducive to a simple solution, but rather calls for numerical or analogue methods. Hence, only in simpler situations is a precise solution for target motion in response to blast to be obtained.

As an alternative to an exact solution for target notion, various empirical estimates of the damage potential of blast have been used. One of these is based on the peak overpressure in the free-field blast wave. For example, it may be stated that a peak overpressure of such and such psi causes major target damage. It should be recognized that such a statement even if correct can at best be only a crude approximation. It ignores the fact that the damage potential of blast is a function of two individual items, the transient blast loading plus the dynamic response of the target; two such aspects are always involved in assessment of damage potential.

A two-aspect criterion for blast damage potential that has met with considerable success is the "critical impulse within a critical time" (Ref. 9). This criterion states that for each possible target there exists some critical impulse above which the target is damaged if such impulse is received within a critical time, but below which there is no effect. The identification and selection of the critical time for any specific target is essentially empirical, but may logically be taken as about one-quarter the natural period of free vibration. The damage potential of the blast for some specific target becomes the net impulse per unit area obtained by time integration of the blast overpressure out only to the specified critical time. This criterion seems a realistic one, and has been shown to agree with direct observations of various damage effects in several circumstances.

An interesting point in connection with this two-aspect criterion is that the ratio of critical impulse to the critical time for any target corresponds to a sort of "critical overpressure" for that target. This critical overpressure can be interpreted as the minimum overpressure capable of causing damage, but which actually would cause damage only if sustained for at least as long as the critical time.

Appendix A

1, KILLOGRAM OF TIVE

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	SIDE-ON		089•	.672	•660	649•	•638	.627	617	. 637	868	.589	ממט		2)(4	• 564	• 557	• 550	775	536	532	1221	\$ 522	53.6	800	500	492	4484	477	69#•	•461	453	5445
	SIDE	PEAK OVERPRESSURE (BARS)	1.403	10333	1,269	1.209	121	760° x	1.045	966*	,951	.908	969		. 832	• 199	• 768	.741	737	695	.677	.661	649•	632	.613	100	.576	•559	244	• 529	.515	• 502	.489
	TN	AVERAGE TRAVEL SPEED (H/MS)	056*	.932	476.	898	•885	.867	.853	048*	. 827	315	400	200	267.	•782	.772	+762	.753	47.	.735	•726	.718	711	703	696	069•	•683	.677	•671	•665	6659	•654
KILOGRAM	SHOCK FRO	TRAVEL TIME (MS)	2.368	2.468	2,570	2.674	2.778	2,883	2.989	3.096	3.204	3,313	7,00	7 1 1 1 1	5.534	3,645	3,758	3,872	3.986	4.102	4.218	4.336	454°4	4.573	4.691	4.811	4.930	5.050	5.171	5,292	5.414	5,537	5,659
HASIS GNE KIL	ŝ	MACH NUMBER	1.484	10404	7.44.0	1.427	1.409	1.393	1.377	1.362	1.347	1.0334	***	1000	1.309	1.298	1.288	1.279	1,270	1.263	1.257	1.252	1.248	cnc.1	1.235	- 208	1.222	1.216	1.211	1.205	1:200	1.196	161-1
23		SCALED DISTANCE (PETERS)	0 0 0	000	25.35	200	2.45	5.0	, v , v , v , v	200	2,65	2.70	ř	200	2.80	2,85	2,90	2.95	4.00	3,05	3.50	3.15	5.20	36. 1	000		5,40	3.45	5.50	5.55	3.60	3.65	3.70

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_ G	OBESTS ONE !	KILOGRAĤ		i a		-	÷	;	•	٠, .	
·	٠	SHOCK FRO	RONT	IS .	SIDE-ON		-	KE	HEFLECTED	c	
SCALED DISTANCE (METERS)	HACH NUMÜER	TRAVEL TIME (MS)	AVERAGE TRAVEL SPEEU (N/4S)	PEAK Overpressure (rars)	URE IMPA	PRESSURL INPULSE DURATION (BAK-MS) (MS)	DECAY PARAKETER	PEAK OVERPRESSURE RATIO	14PULSE (BAR-KS)	VELOC DURAT (KS)	ž.
	1919	5.783	ត្តកំនុ ំ	8478	.437	2-174		केंद्र • ह		2.76	
000°	1.183	5.907	5.43°		925	2,187	ນີ້	1010	######################################	7.7.	
50.5	37	4.1.7		2017	600	0,000	1 d	1001		57.3	
35.95 8.95	1.169	5.282	629	427	400	2.220	a A	00.4		2.80	
4.00	1.104	6.407	.624	.415	.391	2.230	\$5\$.97	1.01	9.80	
4.10	1.156	6.657	•616	293	.375	2.249	55.	16.		2.81	
6.20	1.149	906.9	809	.373	.359	2.267	.52	• 86	-92	28°	
4.30	1.142	7.155	• 602	•356	.346.	2.25%	,51	•82		2.83	
04.4	1.139	7.396	595	946.	0,340	2,368	04•	•7•		2.84	
4.50	1.135	7,637	685.	.336	.335	2.332	•50			2.85	
4.60	1.132	7,879	584	• 328	+332	2,356	64.	°75		24.8b	
4.70	1.130	8.121	625.	.322	•329	2.380	87.	.73		2.5B	
06*# 4*90	1.128	8.365 8.615	.554 .569	.317 .308	.327	2.405 2.429	.48. 547	259.	.75	2.69 2.91	_
5.00	1.121	8,869	494*	666	.317	2445	445	79"		26.92	
) (1.117	9.13	624.	290	311	2.47	940	0690	340	# 5 TO 10	
្ន	1.114	9,39	6554	•281	.305	2.50	54.	.623		0,50	
es es	1.111	9.65	64S*	.273	.298	2,52	5	.607		2002	
2	1-108	9.92	++S.	• 265	+292	2.53	54.3	285°		}•98	
ស្	1.105	10.19	0250	.257	.286	2.54	649	0,570		66*	
5.0	1.102	10.47	.555	•250	.280	2.56	25.	5553		5,99	
5.7	1.099	10.74	.531	472	.274	2,57	***	ອກຸນ	632	3.00	
8°8	1,097	11,02	• 525	.237	.269	5,59	.41			3.0%	
6°0	1.094	11,30	• 522	.231	•264	2.60	Ť'n•	30G*	. 664.	3•01	
6.0	1.092	11.58	•518	-225	.259	23.62	£ th •	264,	. 583	\$•02	
6.1	1.090	11.87	•134	•219	•254	2.63	040	624.		3.03	
6,0	1.068	12,15	.510	.214	.250	2.65	04.	•466	9220	30°50	
	1.086	12.43	507	•203	.247	2.68	040	\$.44°		5.07	
4.0	1.084	12.72	.503	•203	.243	2.71	•39	Tht.		\$.09	

		VELOCITY DURATION (MS)																															
			3.11	3,13	3.16	3.18	3.20	3.22	3.23	3.23	3.24	3.25		3.26	3.26	3.27	3.27	3.28	3.28	3.29	3.30	3,32	3.33	3.34	3.36	3,37	3.38	3°40	3.41	3.42	3.44	3.45	3.47
	REFLECTED	impulse (Bar-MS)	e 683	.521	.513	,507	• 501	464	•486	644.	•472	191		.457	451	555.	.437	•431	454·	•419	.413	+407	*405	.397	.392	*387	• 362	.377	.372	.367	.363	945.	•384
	RES	PEAK OVERPRESSURE RATIO	.430	614.	904.	.398	.38e	•379	.370	.361	352	おまの	•	.336	.329	.321	.314	.307	.302		•289	*88*	.276	.273	•268	.263	25.53	•25¢	64%·	242	142.	.233	.233
		DECAY PARAMETER	6.00	65.	38	.37	•37	•36	•36	30	. 5	.35	2	•35	•35	##.	÷34	•34	¥5.	. 34	.34:	なれる	•34	•34	900	→10.	340	+34		金門	75.	3.34	.33
		SSURE ATION (MS)						-																					.,				
		PRESSURE IMPULSE DURATION faar-MS) (MS)	2.74	2,77	2.80	2.83	2.86	2.88	2.89	2.90	0	10	}	2.94	2,95	2.96	2.97	2.97	2.98	3.00	3.01	3.02	3.04	3.05	3.06	3.05	3.09	3.11	3.12	5.13	3 5	3.16	3.18
	No-	E IMPL	042	237	234	232	•229	.226	222	610	2	110	1	.208	• 204	200	197	.193	•190	187	.184	.182	•179	177	175	173	170	.168	166	164	162	161	.159
	SIDE-ON	PEAK Overpressure (bars)	198	101	189	•185	•180	176	172	169	186	9			154	151	148	145	•142	139	.137	134	.132	130	127	.125	•123	.121	6110	2117		113	.111
	TZ.	AVERAGE TRAVEL SPEED (M/MS)	00%*	767	ħ6ħ•	491	.488	4486	180	481		27.1	•	. 475	.473	471	697	194.	•456	494	-462	.461	094*	853	457	456	757	• 453	284	157	050	957.	244
ONE KILOGRAM	SHOCK FRONT	TRAVEL TIME (MS)	13.03	1 C	13,57	13.85	14.13	14.41	50,00	10.07	ייי	200	CC+CT	15.80	16.08	16.36	16.63	16,91	17.19	17.45	17.73	18.01	18,28	18,55	10.83	19.10	19.37	19,65	19.92	20.10	20.46	20.74	21,01,
BASIS ONE K		HACH NUMBER	\$.080	1080	1.078	1.076	1.075	\$ - n 2.4	1,071	070	200	1.0000	200°T	1.065	1.064	1.063	1,062	1.060	1.059	1.058	1.057	1.056	1.055	1000	1.053	24052	1.051	1.050	1.050	570.4	640.	1.047	1.047
. 		SCALED ()ISTANCE (METERS)	d Ž	4	,	80.9	6.9	,	7.	• •	,	, t	*	7.5	7.0	2.7	a d	i si	8.0	200	0	30	7.8	3.3	2	8.7	8.9	8.0	5		, ,	1 10	.0

Q.	BASIS ONE	KILOGRAM									-
	-	SHOCK FRO	RONT	SIDE-ON	Ş		,	R	REFLECTED		
SCALED DISTANCE (METERS)	MACH NUMBER	TRAVEL TIME (MS)	AVERAGE TRAVEL SPEED (H/MS)	PEAK OVERPRESSURE ABARS)	: IMPUI (BAI	PRESSURE IMPULSE UURATION (BAK-MS) (MS)	DECAY PARAMETER	PEAK OVERPRESŠURĖ KRATIO	IMPULSE (BAR-MS)		VELOCITY DURATION (MS)
Q.	1.646	21.28	93 3	. 109	157			\$220	•350	3,48	,
9.6	3*0*E	21,55	5445		155		.33	35.7		3.50	
4.5	3,045	21.93	かかか。		154		•33	•225		3.51	
9.6	1.044	22.10	6443		152		•33	•219		3.53	
	1.043	22.37	のカオ・シ	٠	151		•33	.216	3000	3,54	
10,0	1.043	22.64	5462	• 102	150	3.26	•33	6213		3,55	
10.1	1.042	22.92	100		148	3.27	• 53	•210	.327	3.57	
10.2	1.042	23.19	044	660	147	3,29	•33.	,207		3.59	
10.3	1.041	23.46	439		146	3.30	.33	•205		3,50	
XO.	1.041	23.73	9E4.	760.	145	3,32	.33	•253	•317	3,62	
10.5	1.040	24.00	437	960•	344	50,000	. 553	•200	.314	3.63	
900	1,000	24.28	75.0	260	543	75.00	25.5	151		3.64	
10.7	1.039	24.55	436	•	141	3.35	.33	.195		3.65	
10.8	1,039	24.83	25.0		140	3.36	33	•192		3.66	
10.9	1.038	25.10	454	160.	•139	3,58	.33	190	•301	3.67	
11.0	1.038	25.38	5433		138	3.39	.33	.187	°298	3.68	
111	1.038	25+66	6433		137	3.40	•35	.185		3.69	
11.2	5.037	25.93	• 432		136	3.41	•32	.183		3.70	
11.3	1.037	26.21	• 431		·134	3.42	•32	181	•289	3.71	
\$** 3.E	1.036	26.48	•431	• 086	133	3.43	•32	•179		3.72	-
5115	1.036	26.76	0430	• 085	132	3.44	.32	.177		3.73	
11.6	1.035	27,03	429	•	131	3,45	•32	•175		3.74	
11.7	1.035	. 27.31	824.		130	3.46	.32	.173		3,75	
11.6	1.035	27,58	• 428		. 129	3.47	• 32	.171	•275	3.76	
11.9	1.034	27.86	427		129	3.48	32	•169		3.77	
12.0	1.034	28-13	•427		128	3.49	.32	.167	•2ö9	3.78	
1201	1.034	26.41	• 426		127	3.50	•32	•166		3.79	
32.2	1.033	28.68	•425		126	3,51	•32	,164		3.80	
12.3	1.033	28.96	• 425 554 555	• 079	\$250 500 500 500 500 500 500 500 500 500	3.52	5.00 61.00 61.00	162	222	3.81	
12.4	1.035	29,23	+2h•		124	3,53	•35	191		3.82	

		VELOCITY DURATION (MS)			•			
	۵		សសសស ស្នេញ ស ស្នេញ ស ស្នេញ ស	2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.	50 50 50 50 50 50 50 50 50 50 50 50 50 5	3.00 8.00 8.00 8.00 8.00 8.00	8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4444 000444 000444
	REFLECTED	: IMPULSE (BAR~MS)	2557 2558 2558 2551 2459	2000 2000 2000 2000 2000 2000 2000 200	233 233 233 233 233	2225 2225 2225 2225 2225 2225 2225 222	214. 214. 214. 215.	.212 .199 .189 .173
	₹ •	PEAK Overpressure R Ratio	665 155 155 155 155 155 155	153 153 154 154 154 154	9444 9444 9444 9444 9444 9444 9444 944		1334	5 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
		DECAY Parametei	ରା ବା ବା ବା ବା ଜ ନ ନ ନ ନ ନ	୯୯୯ ମୁଖ୍ୟ ୧୯୯ ମୁଖ୍ୟ		4444		44400 44400
		PRESSURE IMPULSE DURATION (BAR-MS) (MS)					•	
		PR VLSE DI AR-MS)		22.22.22.22.22.22.22.22.22.22.22.22.22.	646.00 646.00 646.00 646.00	5.50 5.60 5.60 5.70 5.70	4444 444 444 444 444	2 2 2 2 3 3 4 3 5 5 6 6 6 7 6 7 7 7 8 7 8 7 8 7 8 7 8 7 8 7
	SIDE-ON		**************************************	44444 4444 4444 4444 4444 4444 4444 4444	कृष्ण करण सम्मान सम्मान	20000	00000	00000 00000 00000
	SXD	PEAK Overpressure (Bars)	.077 .00. .00. .00. .00.	. 079 . 073 . 073 . 072	.070 .070 .069	. 068 . 064 . 067	0.000 000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.	0.000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000
	. LNO	AVERAGE TRAVEL SPEED (M/MS)	11 12 12 14 14 14 14 14 14 14 14 14 14 14 14 14	**************************************	\$000 P	2995 955 955 955 955 955 955 955 955 955	क्षेत्रके क्षेत्र सम्बद्धाः केल्ड्रिके	# 0 C 0 C 0 C 0 C 0 C 0 C 0 C 0 C 0 C 0
KILOGRAM	SHOCK FRO	TRAVEL TIME (MS)	29.78 30.06 30.33 30.53	30.88 31.15 31.42 31.70	322.52 322.52 33.00 5.00 5.00 5.00 5.00 5.00 5.00 5.0	33.61 34.15 34.15 34.70	34.97 35.82 35.83 36.03 36.03	2000 2000 2000 2000 2000 2000 2000 200
BASIS ONE K		MACH NUMBER	1.00 du	######################################	000000000000000000000000000000000000000	1.0029 1.0029 1.0029 1.0029	1.0028 1.0028 1.0021 7.003	1.027 1.025 1.024 1.022
m	•	SCALED DISTANCE (METERS)	000000 000000 00000	<u> </u>	<u> </u>	OHUND 0-000	មិនក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ស្តេស្ត្រ បាល	20000 20000

~~ . ~~ ~	BASIS ONE	KILOGRAM	11.	5		,· 	- ⁶ 0 -		^ ,		-	
	- -	SHOCK FRO	RONT	IŞ.	SIDE-ON	,	,		S. SEE	REFLECTED		
1.5-	NUMBER	TRAVEL TIME (HS)	AVERAGE TRAVEL SPEED (M/MS)	PEAK. OVERPRESSURE THPULSE DURATION (BARS) (BAR*HS) (MS)	URE THPU	PRE ILSE DÜR IR*KS)	SSURE INTION	DECAY O	PEAK OVERPRESSURE RATIO	Impir.se (bar-ms)		VELOCITY DURATION (MS)
20.0	1.020	50.0	00֥	0470	• 084 032	3.91 3.93		0.0	* 096 * 052	167	4.14 4.14	,
25.50	1.018	300 m	.397	06400	120%	3.45	·	900	190	.156	4-18	
0.0.	1.017	58•1 60•8•1	• 396. • 395	.0410	470.	3.98 4.00		ଦ୍ଧ କୁ ଜଣ୍ଡ	+083 +089	.150	4-19	
25.0	1.016	63.5	468.	.0375	•068	4.01		•28	+076	041.	4.23	
20.0	1.015	00°	.393	•0355	•0656	0°4	`	127	0720	1346	4054	
7.80	1001	100	5.792 191	.0338	0.00	4 =	~{ ,	. 27	5890	1297	4.26	
29.0	1,013	74.2	198	•0305	0578	\$ 000 \$ 2	•		*0618	.1204	4.29	
0.02	1,012	76.9	35£•	•0289	.6553	4.11	ζ*	,23	•0586	.1159	4.3.	
0,10	1.012	79.6	.389	., 0275	¢0259	4012	•	.22	0556	.1116	4.32	
0.70	1.011	82,4	.389	•0260	• 0507	4.14		.20	• 0526	.1075	4.33	
3,000	1.001	85.0	0 0	•0247	*0483	4.16	-	91.	86404	.1035	8.038 3.038	
•				200	•	7	•	074	27.00	9660	0	
35.0 6.55 6.55	1.009	3°00	187	.0221	· 0443	61.4		•16	00446	•0959	4.37	
07	1.008	95.7	286	. 198	1270	200		97	7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2260	7	
6.0	1.008	98.4	•386	.0187	.0388		-	- C	0377	0856	7 7 7	
39°¢	1.008	101.1	• 386	.6177	.0371	4.25	_	òlio Olio	• 0356	• 0825	4.43	
400	1.007	103.8	.385	.0167	.0355	4.26		•16	.0336	•0795	444	
11.0	1.007	106.5	•305	•0158	.0340	4.27	•	16	•0318	.0767	4.45	
o ō	1.006	109.1	.385	0510	.0326	4.28	·	•16	.0301	04200	1.47	
0.5	1.006	111.8	385	00142	.0313	4.30	•	•16	• 0285	•0714	4.48	
0::+:	1.005	114.5	•384	.0134	•0301	4.51	•	,16	•0270	0690•	69.4	
0"51	1,005		.384	.0128	.0289	4.32		16	.0257	.0667	4.50	
460	\$.005		-38t	.0122	.0279	4.33	•	•16	.0245	90900	4.51	
47.0	\$ 000°		185.	00116	•0269	40.4		•16	•0233	•0626	4.52	
0:00	1.00°		.383 	1110-	0250	4.35	•	•16	+0223	•0503	#S.#	
25.6	20004		307	• 070•	2020	4.30	•	116	C120•	*05VI	2000	

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		VELOCITY DURATION (MS)						
			4444 500 500 500 500	4.661 4.661 4.663 4.663	4444	6,69 4,70 4,70 4,71	44444444444444444444444444444444444444	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
	REFLECTED	IMPULSE (Bar-MS)	.0562 .0549 .0549	.0520 .0513 .0508 .0504	.0501 .0503 .0503 .0507	.0518 .0517 .0507 .0497	.0447 .0468 .0468 .0449	.04032 .04036 .04036 .04036
	REF	PEAK Overpressure Ratio	.0207 .0201 .0195 .0191	.0187 .0186 .0187 .0189	.0196 .0202 .0208 .0216	.0233 .0233 .0223 .0227	.0216 .0201 .0206 .0201	.0191 .0165 .0183 .0178
		DECAY PARAMETER	444 444 444 444 444	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	99999 9999 999	9944 994 994 994 994	39999 99999	44444
		SSURE RATION (MS)				-		
		PRESSURE IMPULSE DURATION (BAR-MS) (MS)	# # # # # # # # # # # # # # # # # # #	5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	444 444 444 444 444 444 444 444 444 44	74444 44444	4444 600000 600000	44444 48888 88888
	Ş			.0222 .0220 .0219 .0219	.0223 .0223 .0227 .0231	00243 00243 00243 00238	.0223 .0219 .0214 .0210	.0201 .0197 .0193 .0190
	SIDE-ON	PEAK Overpressure (bars)	. 00.00 . 00.00 . 00.00 . 00.00 . 00.00	• 00093 • 00093 • 0093 • 0094 • 0096	.00098 .0100 .0104 .0107		0100 0100 0100 0000 090	.0099 .0099 .0099 .0099
	IONT	AVERAGE TRAVEL SPEED (M/MS)		ପ୍ରଥମ ଅନ୍ତର୍ଶ ଅନ୍ତର୍ଶ ଅନ୍ତର୍ଶ	2885 2885 2885 1881	 2000000 211111	**************************************	. 3880 . 3880 . 3880 . 4880 . 4880
KILOGRAM	SHOCK FROM	TRAVEL TIME (MS)	130.66 135.2 135.9 141.2	145.6 146.6 149.2 151.9	157.2 152.3 165.5 165.5 167.9	1730.5 175.8 175.8 181.2	1863. 1865.58 1990.5 1914.58	1997.2 2025.8 2055.8 2077.9 2077.8
BASIS ONE		MACH NUMBER	######################################	1000 1000 1000 1000 1000 1000 1000 100	## ## ## ## ## ## ## ## ## ## ## ## ##	1.0005 1.0005 1.0005 1.0005 1.0005	1.0005 1.0004 1.0004 1.0004	######################################
ជា		SCALED DISTANCE (METEKS)	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	55.0 5.5.0 5.0 5.0 5.0	660 682 683 693 693 693 693 693 693 693 693 693 69	655.0 67.0 68.0 69.0 69.0	70.0 71.0 72.0 73.0	75.0 76.0 77.0 78.0

		ONE KILOGRAM	* *	1000 1000 1	","			· - -	-	*	
-1 -2		SHOCK FRON)NC	NO-3015	NO	•	,	132	REFLECTED		-
SHALED DISTANCE (MITERS)	NUMBER	TRAVEL	ÁVERĀGĒ TRAVEL SPEEU (M/MS)	PEAK Overpressure (Bars)	THPULSE OAR-NS	PULSE DURATION BAR-NS). (MS)	DECAY GVE PARAMETER	PEAK GVERPRESSURE ER RATIO	THPULSE (BAR-KS)	* 、	VELOCITY DURATION (RS)
0.00	#00°T	210.5 210.5	000 000 000 000 000 000		0182	50° 4	•16 •16	.0170 .0367	.0393	4.75 7.75	
20.5	000 € 000 €	215.9	000	1800	0176	4 4 20 4	210	64163	60379	4.75	
84:0	1.003	221.3	986		0110	100	16	•0136	•0366	4.76	
0.00	100°4	224.0	380	•	0167	ម្ចាប់ មាន ទាំង	•16 •46	.0153	0350	4.76	
0,18	1.000	229.3	379	•	0161	4.55	. 16 .	.0147	0349	4.76	
8£1•0 851•0	1.003	232.0	\$75°	.0072	0159	4.50 60 60 60 60 60 60 60 60 60 60 60 60 60	•16 •16	.0145	.0363	4:77	
941.0	1.003		.379		0154	4,56	•16	.0140	0333	4.77	
0.760	100°4		975 975		0152	4,57	•16	0100 40100	0328	4.73	
200	1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	245	275 275 276		0148	1.07 1.07	919	\$100 \$100 \$100 \$100 \$100 \$100 \$100 \$100	0380	7.	
				-				2010			
951.0	1,003		.379	Ī	0144	4.57	•16	•0130	2750	4.78	
0 0 0 0	1.003		925	•	5410		91.	6210	•0338	4.78	
2 6 2 8 8 8	700•1		7.00	-	1410	מ מ פ פ	910	1770	0.000	9 5	
0.156	1.003	261.7	97c.	• 0062	0139	4•58 4•58	.16	• 6125	•0296	4.78	
1001	1.063	204.4	.578	.0062	0138	4.58	•16	•0124	.0297	4.78	

Appendix B

1 POUND OF THE

		VELOCITY DURATION (MS)						
	Q	PULSE (PSI=MS)	. 633 . 75 . 75 . 66	000044 000044	2 2 4 4 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	22 22 28 289	**************************************	1376 1420 1420 1411
	REFLECTED	E	139.7 127.3 117.0 108.8	48.44 94.73 92.9	900.9 900.5 900.1 890.7	89 69 69 69 69 69 60 60 60 60	87.51 86.67 86.13 85.31 84.40	83.20 81.67 80.10 78.49 76.83
59 Fr 13.6 PSIA		PEAK DECAY OVERPRESSURE PÅRAMETER (PSI)	14281. 12688. 11257. 9983.	7882. 7044. 6322. 5683.	4656. 4257. 3901. 3582. 3297.	3047. 2829. 2643. 2471. 2307.	2157. 2020. 1897. 1787. 1690.	1601. 1513. 1431. 1355.
59 F		PRESSURE LSE DURATION (MS)	.184 .176 .167 .158	138 1128 116 104	.0084 .068 .063	.056 .076 .076 .119	.145 .201 .201 .263	8000 0000 0000 0000 0000 0000
	SIDE-ON	PEAK GVERPRESSURE IMPULSE (PSI) (PSI-MS)	18.70 17.38 16.29 15:42	14.038 14.038 13.999 13.999	13.81 13.43 12.17 1.05.15	11.02 10.02 10.05 10.753	11.296 11.884 12.516 13.910	######################################
	vi		1614.0 1456.3 1312.5 1182.4 1066.0	963.4 874.6 799.2 732.7 674.2	6224 5329 5329 555 565 665 8	436.0 436.0 385.7 363.92 343.92	324.16 306.16 290.74 276.40 263.68	2551.93 229.47 219.18 209.18
	NT	AVERAGE TRAVEL SPEED (FT/MS)	19.13 18.13 17.21 16.39 15.66	15.00 14.00 13.00 13.00 10.00	122 112-12 11-01 11-01	10.76 10.46 10.18 9.908 9.651	9.408 9.179 6.963 8.758	6.383 6.216 8.057 7.904 7.756
Pound	SHOCK FRONT	TRAVEL TIME (MS)	#50 #30 #80 #80 #80	.060 .066 .072 .078	.092 .099 .116 .114	1110 1110 1156 166	2000 2000 2000 2000 2000 2000 2000 200	722 722 723 723 723 723
BASIS ONE P		MACH NUMBER	10.135 9.633 9.250 8.690 8.257	7.856 7.492 7.167 6.868	6.349 6.126 5.911 5.707	8.20.44 10.03.44 10.03.14 10.03.14 10.03.14	4.5629 4.396 4.299 4.299	4 4 6 00 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
and the second		SCALED DISTANCE (FT)	.65 .75 .75 .80 .85	1.05 1.05 1.05	1.15 1.20 1.30 1.30	44444 0000000	1.465 1.465 1.860 85	44999 80000 80000

	٠, -	Welctity Iburation (MS)							
		ŝ	34.00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4556	15.00 15.00 15.00 15.00 15.00	,556 ,573 ,597 ,632	.760 .724 .746 .766	.799 .814 .829 .844	.8873 .980 .946.
	KEFLECTED	#	75-13 73-38 71-60 69-76 67-89	66.60	66.66 63.30 63.89	62.38 60.17 58.69 56.82 54.82	51.98 50.76 49.75 48.95 48.35	47.96 47.45 45.90 46.37 45.83	200 200 200 200 200 200 200 200 200 200
. VIS	Æ	Plan Overpressum Er (PSI)	1216. 1154. 1098. 2066.	948.7	948.72 839.63 85255	807.48 764.35 721.84 679.67 639.34	601.71 555.89 524.16 50347 474.80	48 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	343.34 326.62 309.88 294.89 280.96
of 13.6 PSEA	}	DECAY PARANETER	· ·	4.72:	, 50,44 40,44	ಕ್ಷಾತ್ರಕ್ಷ ಕ್ಷಾತ್ರಕ್ಷ ಕ್ಷಾತ್ರಕ್ಷ	សមាសម្រ ស្រុក ភូស្គី ស្រុក ភូស្គី	ಬ್ರಾಗ್ಗೆ ಎಂದು ಬ್ರಾಗ್ಗೆ ಎಂದು	งงงงง เรื่อมเบร
59 FF		PRESSURE E DURATION (NS)	## \$\frac{1}{2} The position of the posi	•492 4	5000 5000 5000 5000	0 3 8 0 8 0 8 0 8 0 8 0 8 0 8 0 8 0 8 0	555 555 555 550 550 550 550 550 550 550	66666 66666 66666 66666 66666 66666 6666	664466 664466 664466
	SIDE-ON	OVERPRESSURE IMPUGSE (PSI) (PSI+HS)	116.050 116.050 116.050 116.050 116.050 116.050 116.050	13.496	13.496 13.233 12.997	12.788 12.556 12.558 12.643	12.746 12.647 12.521 12.370 12.193	111-090 111-039 11-1706 11-445	11.0202 11.0202 11.0002 10.066 10.066
	iñ ,		200.50 192.13 174.35 170.71	163.74	163.74 156.49 150.28	143.90 137.77 131.67 1255.57	1114 - 11 104 - 14 99 - 40 95 - 60	90.89 87.19 83.70 77.19	74 74 74 66 66 66 66 66 66 66 66 66 66 66 66 66
		AVEHAGE TRAVEL SPEED (FT/MS)	7.654 7.647 7.645 7.057	6.973	6.973 6.254 6.738	6.625 6.407 6.301 6.197	6.091 5.091 5.091 6.991	00000000000000000000000000000000000000	ທອນຄຸດ ທຸງ ທຸງຄຸດ ທຸງຄາດ ທຸງຄາດ ທ່າ ທ່າ ທ່າ ທ່າ ທ່າ ທ່າ ທ່າ ທ່າ ທ່າ ທ່າ
QNNO	SHOCK FRONT	TRAVEL TIME (MS)	244 244 244 244 244 244 244 244 244 244	**	344	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	44488 64608 66608	2.0	622 641 641 641 641 641 641
BASIS ONE FOUND		MACH	6650 6650 6650 6650 6650 6650 6650 6650	3.364	40000000000000000000000000000000000000	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	2.69 2.69 2.69 2.69 2.69 2.69 2.69	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	00000000000000000000000000000000000000
	-	SCALED DISTANCE (FT)	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	2,400	0.00 5.30 5.30 5.30 5.30 5.30 5.30 5.30	งหญิง ชื่อวิธิกับ รับ	44444 86669 86669	44 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	សម្គាល់ សម្គម ស សម្គម ស សម្គម ស សម្គម ស ស

		VÉLÖCYŤÝ ĎURÁTÍÔN (MŠ)						
	9.	(PSI-MS)	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	#### \$0000 \$0000 \$0000	Particular Particular	Page Service		स्याम्य स्थासम्बद्धाः १८ ५० १० ५० १० १८ ५० १० ५० १० १८ ५० १० १०
	REFLECTEO	••	わけらはんれているようない。	46.15 40.15 39.60 38.60 38.60 38.00 38.00 48.00	37.93 37.35 36.75 35.22 35.62 35.64	222222 222222 222222 222222 222222 22222	325-43 34-65 30-836 30-836 30-836 30-836 30-836	27.65.75 27.65.73 27.65.73 6.65.73 6.65.73
PŠÍA	3 2	PĖAK OVĖMPAESSUKE IER	268114 2268114 22444 2255 2255 2255 2555 2555 2555	212+28 262+53 184-53 184-63 176-45	1658.78 154.65 148.65 148.85 148.85	HANGE STATES OF THE STATES OF	1114 1106 106 106 108 108 108	66.66.66.66.66.66.66.66.66.66.66.66.66.
Fr 1346		ĎĔĊAY Ďaňameteř	\$\$\$\$\$\$\$ \$\$\$ \$\$\$ \$\$\$ \$\$\$ \$\$\$	11.00 to 11.	1468 1468 14664 1453 1453 1468		क्षक्ष करण ज्य	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$
59 £		Přessuře Buratión (MS)	6655 6655 6673 661	690 698 707 715 725	1112 1112 1155 1165 1165	278 29 86 86 87 87 87 87 87 87 87 87 87 87 87 87 87	6657 6657 7777 777	6866 695 9212 9212
	SIDE-ON	SURE IMPULSE (PSI-MS)	10.7443 10.655 10.655 10.440	10.2553 10.2553 10.0743 10.0743 10.055	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	4666 4666 4666 4666 4666 4666 4666 466	0 20 20 20 20 20 20 20 20 20 20 20 20 20	SERENCE SERENC
	νή.	PEAK OVERPRESS (PSI)	561 59455 57455 57464 5464 5464	51.646 49.857 48.146 46.513	442 442 444 444 444 444 444 444 444	445 445 445 445 445 445 445 445 445 445	2000 2000 2000 2000 2000 2000 2000 200	2000 2000 2000 2000 2000 2000 2000 200
	ONT	AVERAĜE TRAVEL SPEED (FT/HS)	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	460 4510 4516 4516 4516 4516 4516	# * * * * * * * * * * * * * * * * * * *	3-88-3-88-3-88-3-88-3-88-3-88-3-88-3-8	######################################
PoUND	SHOCK FRO	TRAVEL TIME (DS)	THE WASHINGTON	, 8640 8640 8640 8640	44000 44000 44000 44000 44000 44000 44000	44444 44444 44444 44444 44444 44444 4444	######################################	
BASIS ONE P		MACH NUMBER	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1.9934 1.869 1.869 1.869	1.6330 1.7935 1.7773	4444 A	444444 9999999999999999999999999999999
		SCALED	44444 88444 886 886 886 886 886 886 886	ម្ភា មួយ	24444 201544	22222 2222 2222 2222 2222 2222 2222 2222	**************************************	\$ 340 00000 00000

æ	BASIS CHE POLND	GWO	, ,		č	65	59 F. 1346 PSIA	æ			
	` -	SHOCK FRO	FRONT	10	SIDE-ON		,	2	REFLECTED		
STALED OTSTANCE (FT)	MACH	TRAVEL TIME (MS)	AVERAGE TRAVEL SPEED (FT/MS)	PEAK OVERPRESS (PSI)	PEAK OVERPRESSURE IMPULSE (PSI) (PSI+MS)	PRESSURE SE DURATION (MS)	DECAY Parameten	PEAK OVERPRESSURE (PSI)	25	PULSE (PSI=HS)	VELOCITY DURATION (MS)
20.	1.651	1.456		25,321	A. 274	ŗ	1.21	. 82.86	26.51	1.62	
9.10	1.899	1.485	3.435	24.724	8.092	.938	1.20	80.03	25.97	1.62	
5.15	1.588	1.513	J. 504	24.143	8.011		1.18	77,59	25.43	4.62	
5.20	1.577	1.541	3.374	23,579	7.936		1.17	75.24	24.90	1.62	
5,25	1.556	1.570	3.544	23,932	7:850		1.15	72,98	24.38	1.61	
05.30	2000 A	1,599	34,415	22.5n1	7,771	.973	1013	70.81	23,83	2.69	
5.00	1.5543	1.628	3.287	25.987	7.692		1-12	50.00	23.37	1.60	
5.40	1.534	1.657	3.259	21.490	7:614		1.10	66.72	22.87	1.59	
5.45	1.524	1.686	3.232	21,009	7.537		1.09	64.81	22°38	1.59	
5.50	1:515	1.716	3,205	20.545	7.461	1,007	1.07	62.97	21.90	1.57	
មា - មា	1.506	1.746	34179	20.098		1.015	1.06	61.22	21.43	1.56	-
5.60	1.497	1,776	3.154	19.667			1.05	59.54	20.97	1.55	
5,65	1.438	1.806	3.129	19,253			1.04	57.94	20,51	1.53	
5.70	974-1	3.836	34105	18.856	7.564	1.000	1.03	50°	20-06	٠. در در در در	
0, 00	1.64.1	1.500	2.031	10.876	7.00.		æń•∵.	A • • • • • • • • • • • • • • • • • • •	70.67	go.	
5.80	1.463	1,897	3.057	18,112	7.020	1.056	1.01	53.59	19.19	1.48	
5.85 5.85	1.456	1.928	3.034	17.763			1:01	52.29	18.94	64.E	
9.00	3 · 4 · 5	1,959	30011	3.T. 4.22	6.920		66	51.01	18.70	540	
0 0	10001	166-7	2,989	17,087	-	1.086	86.	20.17	18.47	1.50	
2•00	1.00 th	2.052	2.967	16.758			-97	48.57	16,24	1.51	
6.10	1.420	2.085	2 . 925	16,121	6.730	1-117	•95	46.25	17.81	1,52	
5,20	1.406	2,149	2.885	15,509		1.137	-92	\$0°	17.40	1024	
6.30	1.393	2.213	2.847	14.922		1-156	69•	47.98	17.02	1.56	
06.9	1.380	2.278	2.63.X	14,362	_	1.176	.87	40.02	16.66	1.57	
5.50	1.368	2,343	2,775	13.828	6.384	1.196	.94:	39.18	16.33	1.59	
6.60	3.356	2.408	2.741	13,319		1.215	.81	36.45	16.02	1.61	
6.70	3,0345	2.474	2.708	12,836		1.235	•78	38.45	15,73	1.63	
6.80	1.334	2.540	2.677	12.379		1.254	•75	33.31	15.48	1.65	
6.90	1.324	2.607	2.646	11.948	6.082	1.273	•72	31.89	15.24	1.67	
7.00	1,324	2,675	2,617	11,543		1•292	464	30.57	15.03	1.69	

																					1								
		VELOCITY DURAT'ON (RS)																•											
		PULSE (PSI-MS)	1.71	1.76	1.79	1.84	1.86	1.89	1.92	1.94	1.97	1.99	2.00	2.02	2.03	900	9 6	2.07	2.08	2.09	2.10	2.11	2.12	2.13	2.13	2.14	2.14	20,00	1
	REFLECTED	Ĭ	14.847	14-552	14.442 14.356	14.295	14.259	14.247	14.260	14.298	14.361	14.206	14-012	13.817	13.024	13.431	130047	12.856	12.666	12.476	12.287	12.098	11.910	11.720	11.507	11.298	11.094	10-894	20000
IA	Ä	PEAK • OVERPRESSURE VER (PSI)	29.356	27.200	26.258 25.405	24.637	23,953	23,352	22,833	22,393	22.031	21.429	20.803	20,205	14.655	19,092	980.44	17,621	17.182	16,769	16.380	16.015	15.675	15:349	14.942	14.549	14017	13,808	100000
F. 15.6 PSIA		DECAY Parame	994	90	58 8	.57	•57	•56	•57	•58	9.0	•59	ຜູ້	-57	3.56	95.	ព្ធ	30	35.	.53	.53	• 54	•54	ញ់ ហិ	.55	• 555	÷24	٠ ا	eg.
98		PRESSURE ILSE DURATION (MS)	## F	1.45	1.37 1.39	04.1	1.42	1.44	1.46	1.48	64-1	1.51	1.53	#	1.55	1.57	000	1.61	1:62	1.63	7667	1.E	1.66	1.67	1.68	1.69	1.69	6. 2.	Lou
	SIDE-ON	URE IMPUL (PSI-HS)	5.94B	5.824	5,767 5,712	5.660	5.611	5,565	5,521	5.480	5.442	5,382	5.317	5.252	5,186	10. 10. 10. 10. 10.	0000	4.927	4.862	4.797	4.731	4.666	4.600	4.333	4.452	4.37:5	4.295	4.223	14104
	SI	PEAK OVERPRESSURE IMPULSE (PSI) (PSI-MS)	11.163	10.481	10.179 9.903	9.653	9.428	9,229	9.056	8.909	6.788	8.584	8.372	297.8	7.970	7.782	7.50 A	7.265	7:109	6.961	6.822	069.9	6.566	6.448	6.298	6.154	6.014	5.070 10.00	2.7.4X
Ξ	ראס	AVERAGE TRAVEL SPEED (FT/MS)	8.00 8.00 8.00 8.00 8.00	2,535	2,510 2,485	2,461	2.438	2.415	2,393	2,372	2.351	2.331	2.312	2.294	2•276	85.50	143.7	2,209	2.194	2.179	2•164	2.149	2.136	2-122	2.108	2.095	2.083	2.070	Z*02%
POUND	SHOCK FRO	TRAVEL TIME (MS)	7.00 4.00	2.88	2.95 3.02	8,09	3,16	3.23	3,30	3.37	3.45	3,52	3.59	3.65	3.74	48.	, k	, d	4,10	4.18	4.25	5000	04.4	84.49	- 55.4	14.63	4.71	4.78	QQ • +
BASIS ONE P		MACH	1.305	1.289	1.281	1.268	1.263	1.258	1,253	1.250	1.0247	1.241	1.236	1.231	1.226	1888	052.7	70201	1.203	1.199	1.196	1.192	1.189	1.186	1.182	1.178	10174	1.171	10101
<u>**</u>		SCALED DISTANCE (FT)		4.0	7.4	7.66	7.7	7.8	۷.٥	9.0	8•1	es Õ	ю. М•	\$°¢	g.8	30 c	0 0	. Q	0.6	3.1	٠ د	9,3	⊅• 6	9.5	9,6	2,7	9 . 8	٠. د	10.01

		VELOCITY DURATION (MS)																			-							
		PULSE (PSI~#S)	21.5	2.16	8.00 5.00 5.00 5.00 5.00 5.00 5.00 5.00	2.17	2.17	2417	2.58	2.18	3	2.19	200		2,20	2.51	2.52	2.21	2.22	2,33	2.53	2.24	2.24	€ 64 64	2°52	ระ เก	92,0	2.20
ä*	REFLECTED	# .	2000 - 01 0000 - 01	10-137	9.959	9.615	9.450	9.176	9,078	6.983	6.693	8.608	8.726		8.50B	8.444	8.384	8.329	8.278	8.211	8.136	8.062	7.989	7.915	7.841	7.768	7,695	7.622
	·RE	PEAK DESAY OVERPRESSURE PARAMETER (PSI)			12,206	199913	505° 13	11.001	10.855	10.716	10.585	10.461	40°04		10-336	9.948	9.867	9.793	9.726	9.621	054°6	9.378	9.257	9-137	9,018	8.900	8.782	G 665
59 Fo 13.6 PSTA	2		សុំ ស ស ស • • •	•52	55 58 58 58	, 52 , 52 , 52	520	155	.51	• \$0	ر دنان دنان	•20	0.40	, ,	, to 0.	84.	23.	94.	948	648	-47	240	£43	34.	4.0	•46	93.	ភ្
65		PRESSURE SE DURATION (MS)	-100 -100 -100 -100 -100 -100 -100 -100	1.73	1.73 1.74	1.74	00 e	1.75 1.76	1.77	1077	1.78	1,79	1.79	, c	1.82	1.62	1.83	1.84	1.85	1.65	1.86	1.87	1.88	1.88	1.89	1.90	1.90	16.1
•	SIDE-ON	PEAK OVERPRESSURE IMPULSE (PSI) (PSI*#S)	4.075		3.878 3.808 8.808	3.746			3.572	3,549			3.492		0.00 to 0.00 t				;		3.378		•				3,233	
,	··Vî		5.52 5.52 5.53	5.585	5.273 5.166	5.064	995.	4.873	4.750	4.596	4.0.4	4.595	0.000 to		000	262.4		4.331	4.305	4.262	40214	4-165	4,117	4.068	4.020	3.972	3.925	3.877
	RONT	AVERAGE TRAVEL SPEED (FT/MS)	\$ 0.00 \$ 0.00 \$ 0.00	2.035	2.015 2.005	1.995	1.985	1.967	1.960	1.952	1.044	1.937	1,930		1,909	1.903	1.896	1.890.	1.883	1.877	1.870	1.864	1.857	1.851	1.844	1.838	1.831	1.825
	SHOCK 'FRO	TRAVEL TIME (MS)	\$ 60 80 80 80 80 80 80 80 80 80 80 80 80 80	5.09	ซูลู เมษา	5.31	200	20°0	5.61	5.69		5.00 5.00	ส ส ซ ซ ซ ซ	} -4	5.50 5.50 5.50 5.50 5.50 5.50 5.50 5.50	6.20	6.28	6.35	6.42	6,50	6.53	6.65	6.73	6.91	68.9	26.9	7.04	7.12
BASIS ONE POUND	-	MACH	4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	1:157	1.154	1.149	1+140	10143	1.140	14538	10127	1.136	4000 T	-	10106	1.130	1.529	1.228	1.128	1.126	1.125	1.124	1.122	1-121	1.120	1.118	1.517	1.116
ίπ.	•	SCALED OTSTANCE (FT,	400 000 000 000 000	10.3	8. 4. 6. 6. 4.30.	10.6	1001	500 000 000 000 000 000 000 000 000 000	11.0	1801	200	11.3	4 ÷) ;	11.0	11.8	11.9	12.0	1201	12.2	12.3	12.4	12.5	X2.6	12.7	12.8	12.9	13.0

		VELOCITY DURATION (MS)												•														
		PULSE (PSI~MS)	2.27	& & & & & &	2.29	80.00	200	200	2.30	•	2		, c	2.31	2,31	2.31	2.32	2.32	2,32	2.36	20,63	2.48	, S	2,52	2.55	500	20.0	2.5 2.73
	REFLECTED	IMPULSE (PSI	7.549	7.404	7.255	7-175	1,0%	A. 943	6.868	*0.	6.720	844	4.576	6.506	6.437	6.368	6.301	6.235	6•169	5.659	5.331	5.047	4.751	4.473	4.230	4.023	3.826	3.483
٧	REF	PEAK OVERPRESSURE (PSI)	0.546 0.433	8.318 8.203	860*8	7.999	7.806	7.712	7.619	7	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7 7 7	190	7.181	7098	7.017	6.937	6.859	6.782	6.086	5.485	4.977	5.5350	4.150	3.836	00 i	3.317	3.105
F. 13.6 PSIA		DECAY	ស ស ស	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	5 1 1 1 1 1 1 1 1 1 1	£4.	n to		4.2	(7 6	Ç (¥ 5	• • • • • • • • • • • • • • • • • • •	187	4.1	14.	.61	.41	04•	•38	35	35	•35	•35	すれる	#P.	50 PO
59 8		PRESSURE LSE DURATION (MS)	1.92 2.92 3.92	1.93	1.94	1.94	1,95	105	1.96	č	1.96	100	769	1.98 1.98		1.99	1,99	8.00	2.00	2.07	2.16	2.22	2.26	2,29	2.33	2.37	2.43	8 0 8 0 8 0
	SŽDE-ON	URE IMPUL (PSI-MS)	3,183	3,131	3.078	3.053	3,027	3000	2.953	0	2000	0000	V 000	2.837	2.844	202	2.770	2.749	2.728	2,559	2.437	2,305	2.154	2,002	1.892	1.796	1.711	1,637
	Sži	PEAK OVERPRESSURE IMPULSE (PSI) (PSI+MS)	3.830 3.783	3.736	3,646	3.605	3.55 1.05 1.05 1.05 1.05 1.05 1.05 1.05 1	0200	0 00 00 00 00 00 00 00 00 00 00 00 00 0		3.410	0/000	7000	3.266	, p	30102	3,163	3-130	3.098	2.802	2.544	2.323	2,0127	1.957	1.816	1.691	1.581	1.484 1.402
	ONT	AVERAGE TRAVEL SPEED (FT/MS)	1.819	1.806	1,794	1.788	1.781	1.00	1.753		1.0757	10/01	1.140	1.734	7.20	1,723	1.717	1.712	1.707	1,658	1.617	1.583	1.555	2.531	1.511	1040H	A . 478.	1.464
GNNO	SHOCK FRO	TRAVEL TIME (HS)	7.20	7,36	7.53	7.61	7.69	7.75	85.	•	8,03	11.00	8.19	8.28 8.36) r	8.52	8.70	8.79	99	10,51	11,37	17,22	13,36	13,89	14,73	15,56	16.39
BASIS ONE POUND		MACH NUMBER	3) file 5) (4) 6) (4) 6) (4)	1.122	1.109	1.108	1.107	1-156	1.104	1	1.102	101-1	1.100	1.099	1 202	1,000	1.095	1.094	1.093	1.085	1.077	1.071	1.065	1.060	1.056	1.052	1.049	1.046
60		SCALED DISTANCE (FT)	न्य () • (म्य हा न्य न	n e	10 m	13.6	13.7	13.8	N C C C C C C C C C C C C C C C C C C C	;	<i>a</i> :	•	a.	क्ष क्ष		01.5	10.8	0,48	0.50	16,0	17.0	18.0	19,0	20,02	21.0	22.0	236	20°50 50°50

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	REFLECTED	IMPULSE (PSI-	1400 1400 1000 1000 1000 1000 1000 1000	3.075	2.053 2.0842	2.733	2.644	70000 0000	2.399	2.328	7.60 V	2.147	2.098	2-053	2.011	1.971	1.933	1.854	1.853	1.804	1.777	1.753	1.523	2.330	10134	.975
**		PIEAK OVEHPRESSURE (PSI)	2.778	200	2.800	2.20H	90 90 90 90 90 90 90 90 90 90 90 90 90 9	0807	1.925	1.865	1.761	1.715	1.675	1.632	1.590	0824	1.473	1.437	1.402	1.369	1.339	1.315	1.092	3690	226	285. 985.
59 Fe .1306 PSIA	C	DECAY	10 to	S FE	32.	32	N. C.	200		# P	100	160	.33	.31	- T	100	30.	•30	•30	•30	•30	. 30	•29	•26	12.	.16 .16
9 6Ś	-	PRESSURE SE DURATION (MS)	0,0 0,0 0,0 0,0 0,0 0,0 0,0 0,0 0,0 0,0	2.61	2.67	2.70 .	2.73	00.00	2.81	80	99.0	3.90	26.2	20.04	2.95	2.96	2.97	2.98	2•99	2.99	3.00	3.00	3.07	3.12	3,18	3.22 3.27
	SIDE-ON	URE IMPUL (PSI-HS)	1.524	1.427	1.382	1.306	1.274	1001	1010	1.166	1014	1001-1	1.081	\$ 059	1.037	1.016	. 670.	.953	.932	-,912	•89¢	.881	.781	•636	533	.377
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•	ONT	AVERAGE TRAVEL SPEED (FT/NS)	1.443.	10450	1.00 4.00 4.00 4.00	166.0	1.387	2000 to 2000 t	1.369	435.	4500 T	1.350	1.346	1.342	0000 H	1.333	1.328	1.325	1.322	1.319	1.317	1.315	1.297	1.285	1,277	1.265
GWO	SHOCK FRO	TRAVEL TIME	0 0	19.7	20°6 21°4	•	7,7	• •	•	\$6.50	7.00	28.9	29.7	•	•	•.	16,00	1.5	35,5	36.4	37.2	38,0		•	•	70.9
BASIS ONE POUND	. •	MACH	1.0041	1.00 t	1.036	1.033	1.032	3000	1.029	1.028	12021	1.026	1,025	1.025	1.024	1.024	1.00 kg	1.022	1.021	1.021	1.020	1.020	-	1.014	1001	1.007
gar		SCALED DISTANCE (FT)	â	ć	00	.	N F	; ;	ະທໍ	940		0,00	0.0	-	N i	О.	00 *M	ø	÷	4B.0	ઢ	ئ	å	å	å	1000

		VELOCITY DURATION (MS)		
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₹.	REF	PEAK OVERPRESSURE IN TER (PSI)	2001 2001 2001 2001 2001 2001 2001 2001	.2579 .2352
59 F. 13.6 PSIA		DECAY	3355 355 355 355 355 355 355 355 355 35	กรอ
28		PRESSURE SE DURATION (MS)	ក្នុក្ស ស្រួល ស្រួ ស្រួ ស្រួ ស្រួ ស្រួ ស្រួល ស្រួ ស្រួ ស្រួ ស្រួ ស្រួ ស្រួ ស្រួ ស្រួ	3.44 444 48
	SIDE-ON	PEAK Verphessure (Mpulse (PSI) (PSI-MS)		2086
	İŞ	PEAK OVERPRESS (PSI)	44. 44. 44. 44. 44. 44. 44. 44. 44. 44.	.1284
•	7.1	AVERAGE Travel speed (FT/MS)	4444 444 6466 6466 6466 6466 6466 6466	1.248
ONE POUND	SHOCK FRONT	TRAVEL TIME (MS)	87.82 1111.6 111.6 111.6 111.6 111.6 111.6 111.6	7000 7000 7000 7000 7000 7000 7000 700
BASIS ONE F		MACH	11.000 10.000 10.000 10.000 10.000 10.000	1
23		SCALED DISTANCE (FT)	44444 444 60000 000 60000 000	180.0 200.0 200.0

Appendix C

ILLUSTRATIVE CALCULATIONS

The scaling laws in their simplest form are adequate for the following calculations.

A. A spherical charge equivalent to 27 pounds of TMT explodes in the ordinary atmosphere. At what distance should a gage be placed for peak side-on overpressures in the order of 50 psi?

Answer: The scaled distance for a peak side-on overpressure of 50 psi is found in Appendix B to be about 3.85 feet. Actual distance by Eq. $10 = 3.85 \times (27)^{1/3} = 11.5$ feet.

B. What is the duration for the positive bade-on overpressure for the blast wave of calculation A?

Answer: From Appendix B, the scaled side-on duration is obtained as 0.698 ms. Actual duration by Eq. 11 = $0.698 \times (27)^{1/3} = 2.1 \text{ ms}$.

C. What positive impulse is anticipated for the gage of calculation A?

Answer: Appendix B lists scaled side-on impulse as 10.16 psi-ms. Actual impulse by Eq. $12 = 10.16 \times (27)^{1/3} = 30.5$ psi-ms.

D. Write an analytic expression for the overpressure time curve for the gage of calculation A.

Answer: From Appendix B, decay parameter b is found as 1.9 (closely) and the duration has been established as 2.1 ms. Hence the term b/t_d of the exponent for the decay relation of Eq. 1 becomes 1.9/2.1 = 0.9. Substituting

overpressure = $50(1 - t/2.1)e^{-0.9t}$

where t is the time (in milliseconds) after the blast wave strikes the gage.

E. What peak overpressure would be felt by a gage at the same distance of 11.5 feet, but 1, that is part of an unyielding surface face-on to the blast wave of calculation A? Compare with the side-on value.

Answer: At the specified scaled distance of 3.85 feet, the peak reflected overpressure is given directly in Appendix B to be about 205 psi. This compares with the side-on value of 50 psi and corresponds to a reflection coefficient of 4.1.

F. A peak side-on overpressure of 59.5 psi is recorded as a distance of 10 feet from an explosion. What is the indicated equivalent yield, in pounds of TNT?

Answer: This peak side-on overpressure corresponds by Appendix B to a scaled distance of 3.60 feet. Then, by the yield equation, Eq. 14,

equivalent yield =
$$\left(\frac{\text{actual distance}}{\text{scaled distance}}\right)^3$$
 = $(10/3.6)^3$ = 21 pounds TNT

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Two rather distinct types of blast are conventional explosion. One is a close explosion products and air; the other is atmospheric air only. These two types quantitatively in terms of a reference spherical charge of unit mass of TNT in for explosions which are geometrically and their limitations carefully cutling illustrated by numerical examples. The important aspects and makes it difficul analytic means in any except the simple need for semi-empirical methods such as within a critical time. Detailed table explosions (Appendixes A and B) give va characteristics, and travel and duratio for both free-field and normal reflecti	e-in composite best are described and composite best are described and control	last the blast scribed en here tmosphered from the appire of bits damaged from the control of th	at involves both that involves qualitatively and as that of a bare re. The scaling laws om basic principles, lications are last is one of its age potential by ce, there is still impulse delivered of blast from reference
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